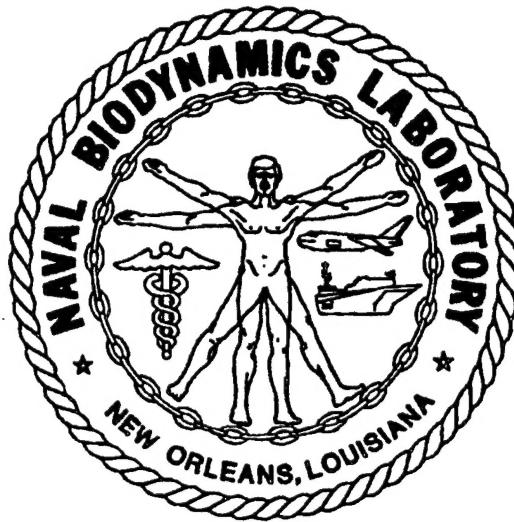


Naval Biodynamics Laboratory
NBDL-86R007

**DYNAMIC VARIABLE AND TEMPORARY INJURY CORRELATION
FOR HUMAN HEAD AND NECK IMPACT EXPERIMENTS**

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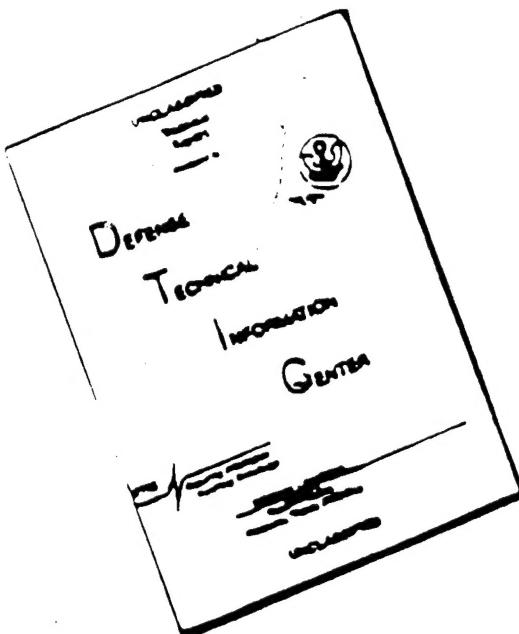
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DYNAMIC VARIABLE AND TEMPORARY INJURY CORRELATION FOR HUMAN HEAD AND NECK IMPACT EXPERIMENTS

BRIAN W. WAMSLEY, ALVAH C. BITTNER, JR., NORMAN S. GILBERT,
LEONARD S. LUSTICK

ABSTRACT

The Naval Biodynamics Laboratory (NBDL) has collected a data base describing the head/neck kinematic response of a large number of human subject volunteers to -X, +Y, and -X+Y vector exposures. This paper will present injury-related parameters for the most severe exposures in each vector, together with correlations of these parameters with the medical findings. The parameters presented include axial and shear forces and torques at the occipital condyles, as well as the head injury criterion (HIC number). Moderate ($R = .35$ and $.38$) but highly significant ($p < .025$) correlations were revealed between general (GENFAC) and muscle (MUSFAC) symptom factor variables. These findings encourage continued systematic evaluation of the relationship between the observed injury-related (eg. axial and shear) and medical findings.

INTRODUCTION

The Naval Biodynamics Laboratory (NBDL) has collected a data base describing the head-neck kinematic response of human subject volunteers to -X, +Y, and -X+Y, vector exposures. The goal of this program has been to develop human dynamic and injury response models to impact acceleration as well as to determine the correlation of dynamic responses with physiological effects and injuries. This information is in use for design, construction, and validation of manikins and mathematical models. These products are used to evaluate human protective systems for prevention of casualties from severe impacts (e.g., aircraft crashes and ejections). Thomas, Ewing, Majewski, and Gilbert (1) have previously reported modest correlation between clinical medical effects and sled acceleration and direction. Interestingly, current as well as previous modeling efforts predict that such correlations would be greater, if correlations were made relating "injury-related variables" (eg., maximum shear) with clinical variables (eg., Ewing et al. (2) and Muzzy et al. (3)). This paper will present injury-related parameters for maximum -X,+Y, and -X+Y exposures and their correlations with medical findings.

METHOD

Subjects--The subjects were six Navy enlisted men (ages 19 to 23) who had volunteered for duty as biodynamics research subjects (ie., subjects H131 to H136). They had been selected to be unusually free of skeletal, cardiopulmonary and other medical or psychological conditions which would preclude participation in potentially hazardous environmental research. The subjects were otherwise typical of the general enlisted population. All subjects were recruited, evaluated, and employed in accordance with SECNAV Instruction Series 3900.39 and MANMED Instruction Series 3900.6.



These instructions are based upon informed voluntary consent and meet the provisions of prevailing national and international guidelines regarding proper human experimentation. A more detailed description of the volunteers and their selection is given by Thomas, Majewski, Ewing, and Gilbert (4). Tables 1 and 2 respectively contain selected measured and estimated anthropometric parameters for the volunteer subjects.

APPENDIX

Tables 1 and 2 about here

Experimental Design -- Subjects were exposed sequentially to blocks of G(-x), G(+y) and G(-x+y) sled profiles with respective maximums of 15, 7 and 9Gs. To minimize the effects of initial conditions each subject was always run in the neck-up, chin-up condition which is standard at NBDL (Ewing et al. (5)). Subjects were medically examined by a physician immediately prior to, shortly after, and 24 hours postrun (or until the abatement of any significant medical findings). This information was recorded for later computer analysis. Retrospective review of the post run medical log yielded five categories of symptoms and physical findings in keeping with that reported by Ewing et al (2). These were (1) hours of muscle soreness; (2) hours of muscle stiffness; (3) hours of headache; (4) hours of backache, and (5) other.

Apparatus -- An Bendix Hyge(R) pneumatically driven .3048m diameter accelerator was used to accelerate an approximately 1.2m by 3.7m multivectorial sled which was rail mounted on Delrin AF(R) pucks. The acceleration stroke is limited to 1.52m and sled mounted brakes were not used. The effective drag is about .2G and the sled was allowed to coast to a stop. Total rail length available is 2.13m. The impact direction (-X,+Y or -X+Y) was determined by rotation of the multivectorial sled.

The subjects were restrained in a nominally upright position by shoulder straps, a lap belt and an inverted "V" pelvic strap tied to the lap belt. Upper arm and wrist restraints were used to prevent flailing. Figure 1 illustrates the basic restraint system which was used for the three vector directions.

Figure 1 about here

Experimental Measurements -- The dynamic variables presented in this paper were derived by integrated accelerometer and cinephotographic measurement systems (Seemann and Lustick, (6)). The accelerometer system yielded measurements using nine piezoresistive accelerometers mounted on a "T" shaped plate at the mouth and six accelerometers mounted on a T-plate at the spinous process of the first thoracic vertebral body (T(1)). The configuration of the accelerometers on the T-plate and the error propagations associated with this method for determining linear displacement, velocity, acceleration and angular orientation, angular velocity and angular acceleration components of a rigid body have been described (Becker and Willems, (7)). The cinephotographic system with the accelerometer system has been previously described (Becker, (8)).



In order to compare subjects at similar points in the anatomy, it is required to define a head anatomical coordinate system and a T(1) anatomical coordinate system (Thomas, (9)). These anthropometric coordinate systems are related to the instrumentation coordinate systems by three-dimensional x-ray anthropometry on each subject (Ewing et al. (5)).

ESTIMATING ANTHROPOMETRIC PARAMETERS FOR THE HEAD AND NECK

One reference frame for the entire series of experiments is fixed to the laboratory. This is established by first defining a sled coordinate system in which the origin is a benchmark permanently machined into the sled structure. The +X axis is parallel but in the opposite direction to the thrust vector of the accelerator. The +Z axis is parallel to gravity and positive upward and the +Y axis is established so that the axes form an orthogonal right hand system. A second frame of reference is fixed to the anatomical axes of the head as illustrated in figure 2. (cf Thomas, (9) for more detail). Both coordinate systems used in this study are right handed where X, Y, and Z axes are taken in that order.

ABY SIGNIFICANT MEDICAL FINDINGS. THIS INFORMATION WILL BE PROVIDED IN A SEPARATE REPORT.

Figure 2 about here. A dynamic head-neck model was developed by the University of Michigan. The model was based on the Head-Neck model developed by Ewing et al. (5).

It should be made a scilicet the head-neck model is based on the Head-Neck model developed by Ewing et al. (5).

Injury-related variables which will be tabularly reported for all runs include maximum and minimum:

~~AN~~>Linear force components (relative to head X, Y, and Z) over a sled run across the head-neck junction (condyles) at approximately 100 km/h in a multivectorial sled which was rail mounted on Lehigh AVT sleds. The accelerations during the sled run were measured and the sled mounted sensors were used.

~~AN~~>Torque components (around the head X, Y, and Z) and resultant forces at the head-neck junction.

HIC component and resultant value for window widths of less than 200 ms. a lap belt and shoulder belt restraint system. The head-neck model and injury variables will be described in detail.

Additionally, the head-neck model will be used to predict the responses of the subjects to the sled runs. In addition, plots comparing the time course for these variables for the subjects with the greatest and smallest head mass parameter (H132 and H135) will be provided for illustration of the range of responses. Time courses for these and other selected variables will be graphically provided for a typical subject (H134). Only linear and torque force components will be related to the medical log symptoms by correlational analysis.

RESULTS

Evaluation of the data was conducted in three phases. During the first phase, dynamic variables believed to be injury-related were examined. Medical variables were analyzed during the second phase. The third phase was concerned with correlation of the injury-related variables and medical variables.



Injury-Related Variables.

Injury-related dynamic variables were tabulated and graphically analyzed during this phase of evaluation. Graphical analysis revealed, as might be expected that the injury-related variables tended to increase in magnitude with increasing exposure (G) levels for the three vector directions. Figures 3, 4, and 5 illustrate time courses for respective changes in the resultant force, resultant torque and HIC variables for a range of 10.2 to 15.6 G(-X), 5.3 to 7.0(+Y), and 9.3 to 11.4(-X+Y). It should be pointed out that, occasionally, experienced forces may be substantially greater for a relatively lower sled G level than at higher levels for the same subject (e.g., H132 at 13 vs. 15 G(-x) in Appendix A). The trend toward increasing injury-related magnitudes with increased exposure limits focused our attention toward the higher levels in later analyses.

Figures 3, 4, and 5 about here

Graphical analyses also indicated that individual differences play a role in experienced forces under nominally the same sled force conditions. Figures 6, 7, and 8 show shear and axial forces as well as resultant torque time-courses for subjects with greatest (H135) and least (H132) head mass parameters. Over nominal 15G(-x), 7G(+y) and 10G(-x+y) conditions, the largest headed subject (H132) tended to experience greater stresses than the smallest subject. The larger subject, as will be seen later, also reported greater medical problems post-run. The apparent role of individual differences focused our attention on their importance in later analyses.

Shear and axial forces as well as resultant torque time-courses for subjects with greatest (H135) and least (H132) head mass parameters. The largest headed subject (H132) tended to experience greater stresses than the smallest subject. The larger subject, as will be seen later, also reported greater medical problems post-run. The apparent role of individual differences focused our attention on their importance in later analyses.

Figures 6, 7, and 8 about here

The results of graphical analysis suggested tabulating experienced injury-related variables for the greatest experienced level for each vector and each subject. The appendix contains a portion of this tabulation.

Medical Variables

The medical variables were tabulated and analyzed during the second phase of evaluation. Table 3 provides the basic data by subject and run. Examining this table, it may be noted that some runs were uneventful while other runs resulted in clusters of symptoms (muscle soreness and muscle stiffness tend to go together). It may also be seen that about 30 percent of the impact runs resulted in some significant symptom. The nature and frequency of such findings were similar to that reported by Thomas et al. (1) where significant symptoms were reported for about 40 percent of the runs. This clustering of symptoms suggested condensing the symptoms into "factors" which are more syndrome in character.

Table 3 about here.



A principal factor analysis was conducted on transformations of the variables shown in Table 3. The first four variables (hours of muscle soreness, through hours of backache) were transformed ($\log(x)+1$) to reduce skewness and theoretically enhance linearity. The last variable was coded as "0" or "1" to respectively denote the absence or presence of other symptoms. The transformed variables are subsequently labeled MUSOR, MUSIF, HEAD, BACK, and OTHER for purposes of identification. The analysis resulted in evidence of a strong first factor (syndrome) which accounted for 50.8% of the variance across the symptoms (eigen-value of 2.53). A second factor (syndrome) was also suggested which added an additional 25.4% of the variance (eigen-value of 1.27). For purposes of this investigation, it was decided to consider results for both the one and two factor solutions with the injury-related variables. Table 4 provides the intercorrelation of the medical variables as well as their loadings (correlations) on the derived factors.

TABLE 4 about here.

The factor from the first solution we termed GENFAC. Those from the second were respectively termed MUSFAC and OTHRFAC. These terms were selected to reflect the relative prominence of general, muscular, and other symptom loadings on the respective factors (cf, Table 4).

Correlation of Medical and Injury-Related Variables

Stepwise regression analysis was applied to each of the three medical factor variables (i.e., GENFAC, MUSFAC and OTHRFAC). Interestingly, prior to the analyses, it had been planned to force specific variables (Maximum Shear, and absolute Axial Forces); however, these were selected from GENFAC and MUSFAC by the stepwise procedure. We also correlated G-level with these factor variables, but maximum shear or axial force showed a higher correlation. For OTHRFAC, the Shear and Axial Variables were unpredictable and a broad range of other variables were considered (e.g. Torques at the condyles, etc.). Analyses for GENFAC and MUSFAC represent planned analyses while that for OTHRF was exploratory.

GENFAC.

Regression analysis with the shear and axial variables yielded a significant multiple $R = 0.354$ ($F(2,57) = 4.07$, $p < .025$). The prediction equation is :

$$\text{GENFAC} = -.7194 + .0027Z + .0028S \quad (1)$$

where Z is the greatest negative axial force (Newtons) and S is the maximum shear (Newtons). The coefficient for Z and S significantly exceeded their respective standard errors ($F(1,57) = 5.20$, $p < .05$ and $F(1,57) = 7.83$, $p < .01$). Equation (1) predicts an increasing GENFAC with increasing sheer force and lessening of the axial force which tends to hold the head on the neck.



MUSFAC. Regression analysis with the axial and sheer variables yielded a significant multiple $R^2 = 0.378$ ($F(2,57) = 4.75$, $p < .012$). The prediction equation is:

$$\text{MUSFAC} = -8.8435 + 0.0025Z + 0.0029S$$
 the abd(2)-rc of exposure to the symmetrical. The transformed variables are substituted in equation (1) to yield:

where Z and S are as defined for equation (1). Again the coefficient for Z and S significantly exceed their respective standard errors ($F(1,57) = 4.44$, $p < .05$ and $F(1,57) = 8.26$, $p < .01$). Equation (2) predicts increases in MUSFAC under conditions similar to that of (1).

or the variance (square-root of the sum of squares of the residuals) of the regression equation is 1.12. The prediction equation is:

It was decided to conduct further analyses on the OTHRFAc variable.

OTHRFAC

No significant relationship was found between OTHRFAc and the torque variables.

Initial regression analysis with axial and shear forces yielded no results of consequence. Subsequent stepwise analysis was only relatively more productive; the best single predictor was the maximum torque about the X-axis ($R = .18$, $p > .16$) which even in conjunction with a second predictor (greatest negative torque about the S-axis) yielded no improvement ($R = 0.236$, $p > .19$). The resulting OTHRFAc prediction equation weight for the torque variables were in the direction of increasing with increasing torque magnitude.

DISCUSSION

This report considered the relationship between variables believed to be injury-related and their correlation with medical findings over (-X), (+Y) and (-X+Y) impacts. Initial analyses focused upon relationships within the medical variables. These focused our attention on the relationship between the injury-related and medical factor variables. Our discussion of these results will follow this pattern of analysis and will precede conclusions.

Injury-Related Variables.

The graphical analyses of these variables revealed two relationships. First and not unexpectedly, the injury-related variables tended to increase with the nominal magnitudes for each vector direction exposure (cf., Figure 3, 4 and 5). This focused attention on the nominally most severe runs for each vector direction in the NBDL database.

The second finding of the graphical analyses was the apparent relationship between the injury-related criteria and anthropometry (i.e., head mass) seen in Figures 6, 7 and 8. Subject H132 with the largest head mass experienced larger forces and torques than the smallest (H135). These subjects also differed on other variables in a similar pattern (e.g. neck length) and consequently the observed systemic differences can not be uniquely ascribed to head mass. (However, the report by Muzzy et al. (3) certainly indicates a strong relationship between head mass and resultant forces and torques.) Interestingly subject H134, with an intermediate head mass reported no adverse effects and had a particularly short neck.



Currently, we are initiating correlation of variables across subjects in an effort to be more definitive. Certainly, these results point to consistent individual differences which are embedded in our later analyses.

Medical Findings

where H and S are as defined above. The results of the correlation analyses and Summary of the medical findings revealed apparent clusters of reported symptoms (cf, Table 3). These clusters could reflect subject tendencies to complain; subject differences in "injury"; or a combination of both. The tendency for subject H132 (largest head mass) to report more often than H135 (smallest) did give some initial support for the view that actual injury differences are involved. Factor analysis was performed to identify and condense the symptoms prior to correlation analyses with the injury-related variables. Table 4 standarized the correlation between the transformed medical variables and factors which resulted from this analysis.

Regression Analyses

The correlational analyses relating the medical factors and injury-related variables provided strong evidence of their relationship. Both the GENFAC (general) and the MUSFAC (muscle) factor variables exhibited moderate but highly significant ($p < .025$ and .012 respectively) correlation with the same shear and axial forces experienced by the subject ($r = .35$ and .38). The prediction equations for these two variables were also similar equation (cf, equations (1) and (2)). These similarities, were in part not unexpected as GENFAC may theoretically be viewed as a comparison between MUSFAC and OTHRFAC. However, the correlation bewteen MUSFAC and GENFAC was relatively higher than expected ($r = .86$). In any case, the relationship between the injury-related dynamic variables and the medical reports is supported by the results in the paper. The choice of symptom cluster does remain open for future work.

CONCLUSION

The findings of this report encourage continued systematic evaluation of the relationship between observed injury-related variables and medical findings. Certainly, the results of this report indicate a moderate but highly significant correlation between reported symptoms and the maximum shear and greatest negative axial forces. Based on this report, additional correlation analyses relating individual differences in anthropometric variables (head and neck size) with the injury-related and medical variables appears a fruitful direction for future work. Perhaps equally productive might be correlation of such variables and injuries experienced by civilian and military personnel in impact environments. We encourage other researchers to focus on non-permanent symptoms following impacts and their relationship with subject variables.



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Aerospace Medicine Research Program
Anthropometry & Ergonomics Division
Subject Status in Aerospace Medicine Division

Table 1. Subject Anthropometric Variables

Subject	Age (Yrs)	Height (cm)	Weight (kg)	Head Circumference (cm)	Head Length (cm)
H131	20	167.0	67.7	57.5	19.6
H132	21	172.9	80.0	57.9	19.7
H133	20	161.7	61.4	56.1	19.4
H134	20	178.3	75.5	56.6	19.4
H135	23	171.6	69.1	53.5	17.9
H136	19	185.4	89.1	56.4	19.4

Table 2. HEAD MASS PARAMETERS

SUBJECT	MASS* (gm)	CENTER OF MASS** (cm)			PRINCIPAL MOMENTS** OF INERTIAL (Kg-cm ²)		
		X	Y	Z	X'	Y'	Z'
H131	4449	0.84	-.06	3.17	219.8	235.0	152.9
H132	4523	0.84	-.06	3.18	225.9	241.5	157.2
H133	4170	0.82	-.05	3.10	197.3	211.0	137.3
H134	4278	0.83	-.05	3.13	205.9	220.1	143.3
H135	3791	0.80	-.05	3.00	168.3	180.0	117.1
H136	4235	0.83	-.05	3.12	202.4	216.4	140.9

*Mass estimated from head circumference and length (Kaleps et al., 1984)

**Center of mass and principal moments estimated via isometric analysis (Bittner, 1986)



RUN NUMBER	SUBJECT NUMBER	G level	MUSCLE SORENESS (HOURS)	MUSCLE STIFFNESS (HOURS)	HEADACHE (HOURS)	BACKACHE (HOURS)	OTHE (YES/N)
3908	H131	10.2G(-x)					
3948	H131	13.7G(-x)					
3987	H131	14.5G(-x)					
3990	H131	15.4G(-x)					
4089	H131	5.1G(+y)					
4109	H131	6.2G(+y)					
4124	H131	7.2G(+y)					
4242	H131	7.3G(-x+y)					YES*
4251	H131	10.2G(-x+y)					YES*
3989	H132	10.3G(-x)	59	59			
3950	H132	13.6G(-x)	68	68			
3957	H132	14.7G(-x)	33	33	7		
3982	H132	15.6G(-x)	49	49		4	
4090	H132	5.1G(+y)	67	67			
4110	H132	6.1G(+y)	70	70			67
4128	H132	7.1G(+y)	47				
4261	H132	9.0G(-x+y)					
4297	H132	10.0G(-x+y)					
4306	H132	11.1G(-x+y)	48		33	48	YES*
3998	H133	10.2G(-x)					
3951	H133	13.4G(-x)					
3963	H133	14.5G(-x)					
3986	H133	15.6G(-x)					
4093	H133	5.1G(+y)					
4111	H133	6.1G(+y)					
4125	H133	7.2G(+y)					
4236	H133	7.3G(-x+y)	44	44	6		
4240	H133	9.1G(-x+y)	95	95	2		
					11		
3993	H134	10.2G(-x)					
3961	H134	13.4G(-x)					
3968	H134	14.3G(-x)					
3983	H134	15.6G(-x)					
4097	H134	5.0G(+y)					
4112	H134	6.1G(+y)					
4126	H134	7.1G(+y)					
4264	H134	9.3G(-x+y)					
4298	H134	10.1G(-x+y)					
4307	H134	11.4G(-x+y)					

* two premature ventricular contractions after impact
** right bundle branch block for three complexes impact
*** felt "stunned" after impact, complained of dizziness for 2 days

RUN NUMBER	SUBJECT NUMBER	G level	MUSCLE SORENESS (HOURS)	MUSCLE STIFFNESS (HOURS)	HEADACHE (HOURS)	BACKACHE (HOURS)	OTHER (YES/N)
3916	H135	10.3G(-x)					
3955	H135	13.6G(-x)					
3965	H135	14.6G(-x)			18		
3970	H135	15.6G(-x)					
4095	H135	5.2G(+y)					
4114	H135	6.1G(+y)					
4131	H135	7.3G(+y)	44		44		
4314	H135	9.1G(-x+y)					
4316	H135	10.1G(-x+y)					
		10.2G(-x)					
4918	H136	10.2G(-x)					
3953	H136	13.3G(-x)	33		20		
3962	H136	14.1G(-x)	47		33		
4098	H136	5.1G(+)			47	47	
4142	H136	6.0G(+y)					YES*
4153	H136	7.1G(+y)					
4247	H136	7.1G(-x+y)					
4263	H136	9.2G(-x+y)	240				

*** one premature ventricular contraction 22 seconds after impact



TABLE 4. MEDICAL VARIABLE INTERCORRELATIONS AND FACTOR LOADINGS

MEDICAL VARIABLES					ONE FACTOR SOLUTION FACTOR	TWO FACTOR SOLUTION	
MUSOR	MUSIF	HEAD	BACK	OTHER	(GENFAC)	(MUSFAC)	(OTHRFAC)
1.000					.856	.901	.169
.800	1.000				.775	.929	-.032
.498	.412	1.000			.797	.549	.629
.402	.286	.588	1.000		.717	.403	.715
.046	-.114	.250	.289	1.000	.232	-.232	.823

MEDICAL VARIABLES CORRELATED IN ACCORDANCE WITH TABLE 4



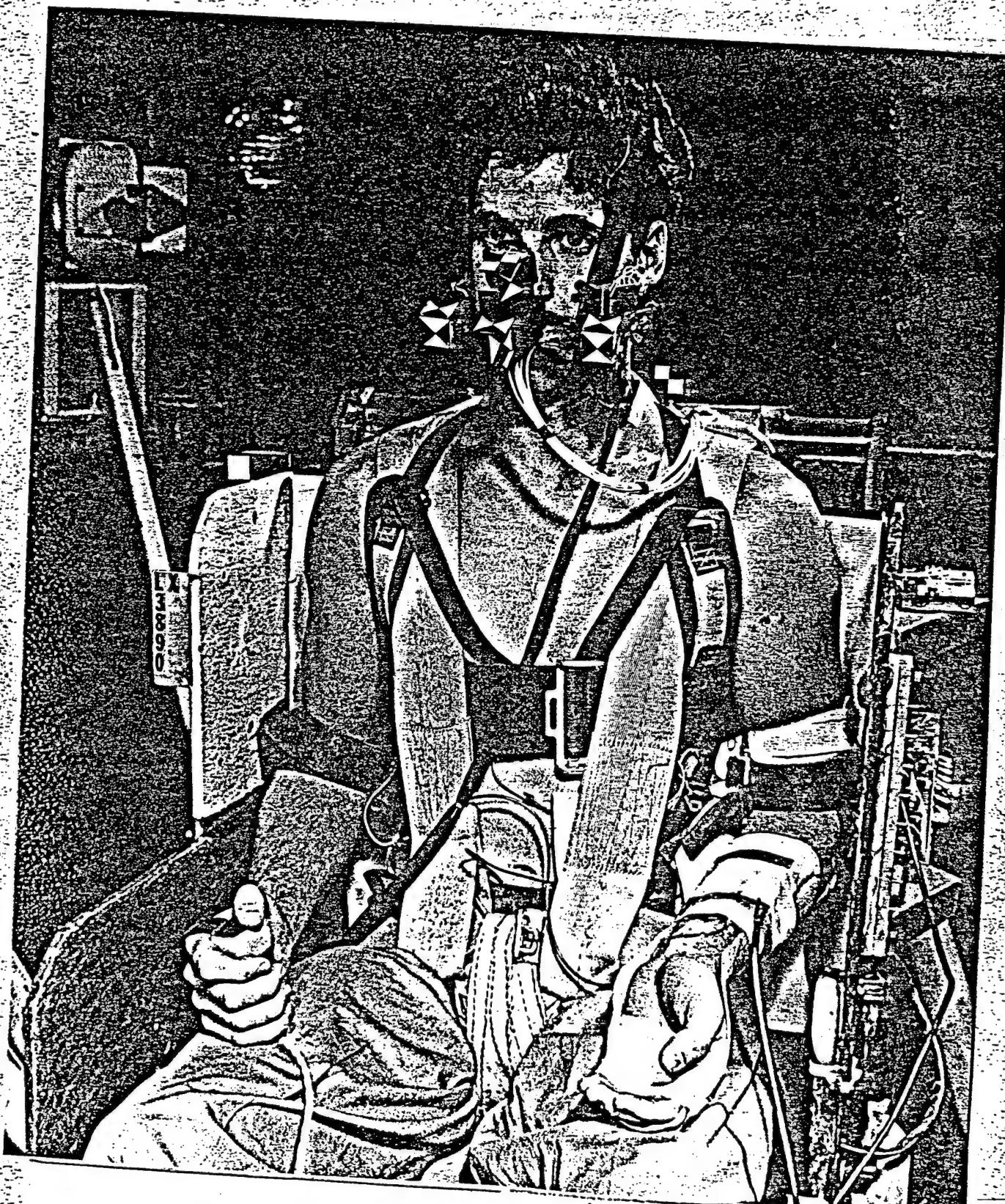
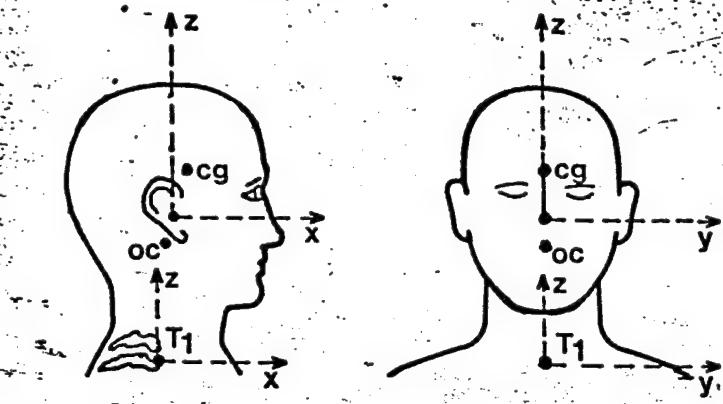


Figure 1, Illustration of the Restraint System as implemented on Subject H134.





**FIGURE 2. HEAD AND T1 ANATOMICAL
COORDINATE SYSTEMS**

**Figure 3. Resultant Force Time-Courses Across -X, +Y, And -X+Y
Vector Directions And Selected Accelerations For H134**

COORDINATE SYSTEM



RESULTANT FORCE FOR MINUS X SLED RUNS

LEGEND	
LX3993	R.J.FORE H00134 10.170
LX3961	R.J.FORE H00134 13.405..
LX3968	R.J.FORE H00134 14.316..
LX3983	R.J.FORE H00134 15.586..

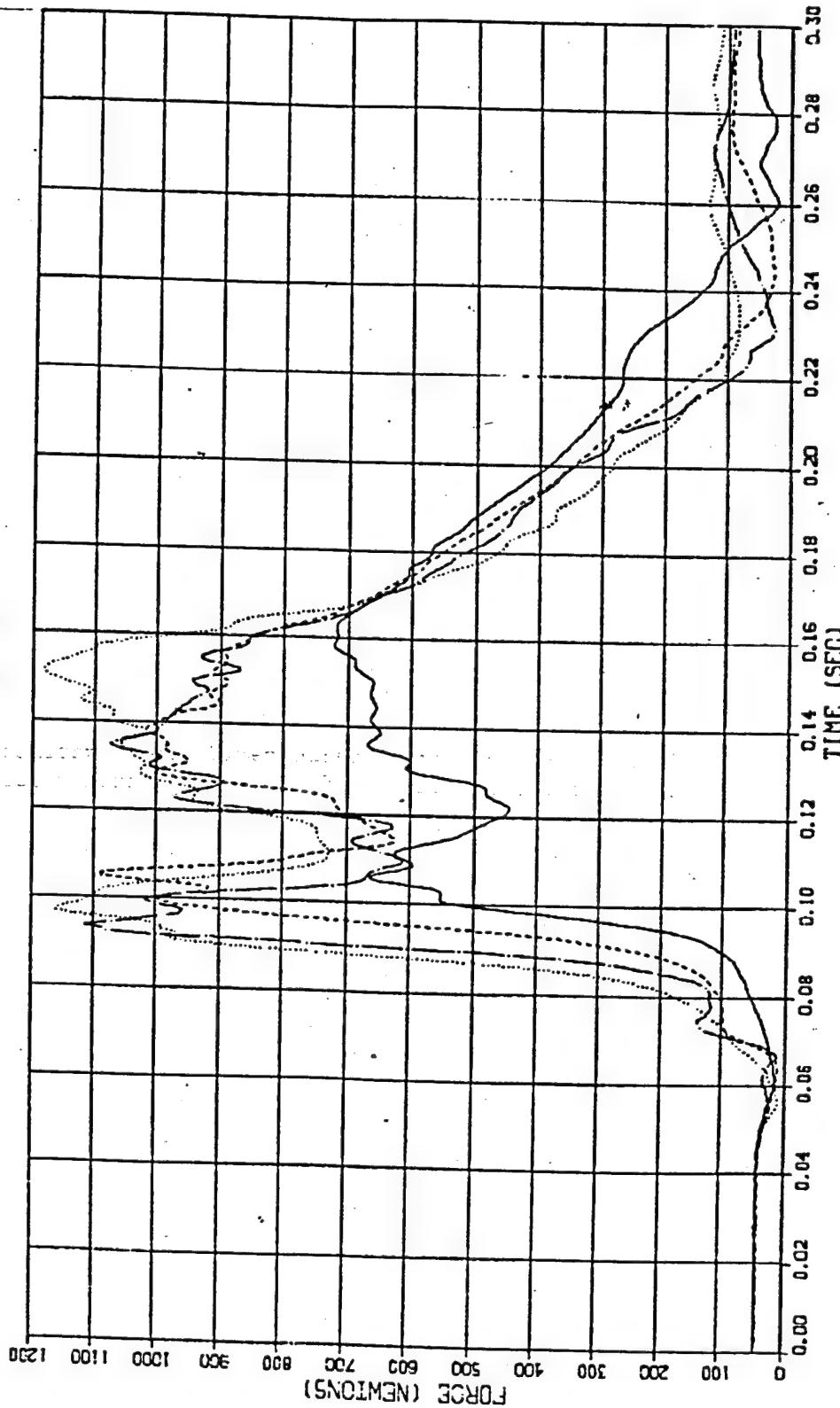


Fig 39

RESULTSANT FORCE FOR PLUS Y SLED RUNS

LEGEND			
LX4097 RJJFORE	H00134	5.02G	
LX41112 RJJFORE	H00134	6.11G	
LX4126 RJJFORE	H00134	7.08G	

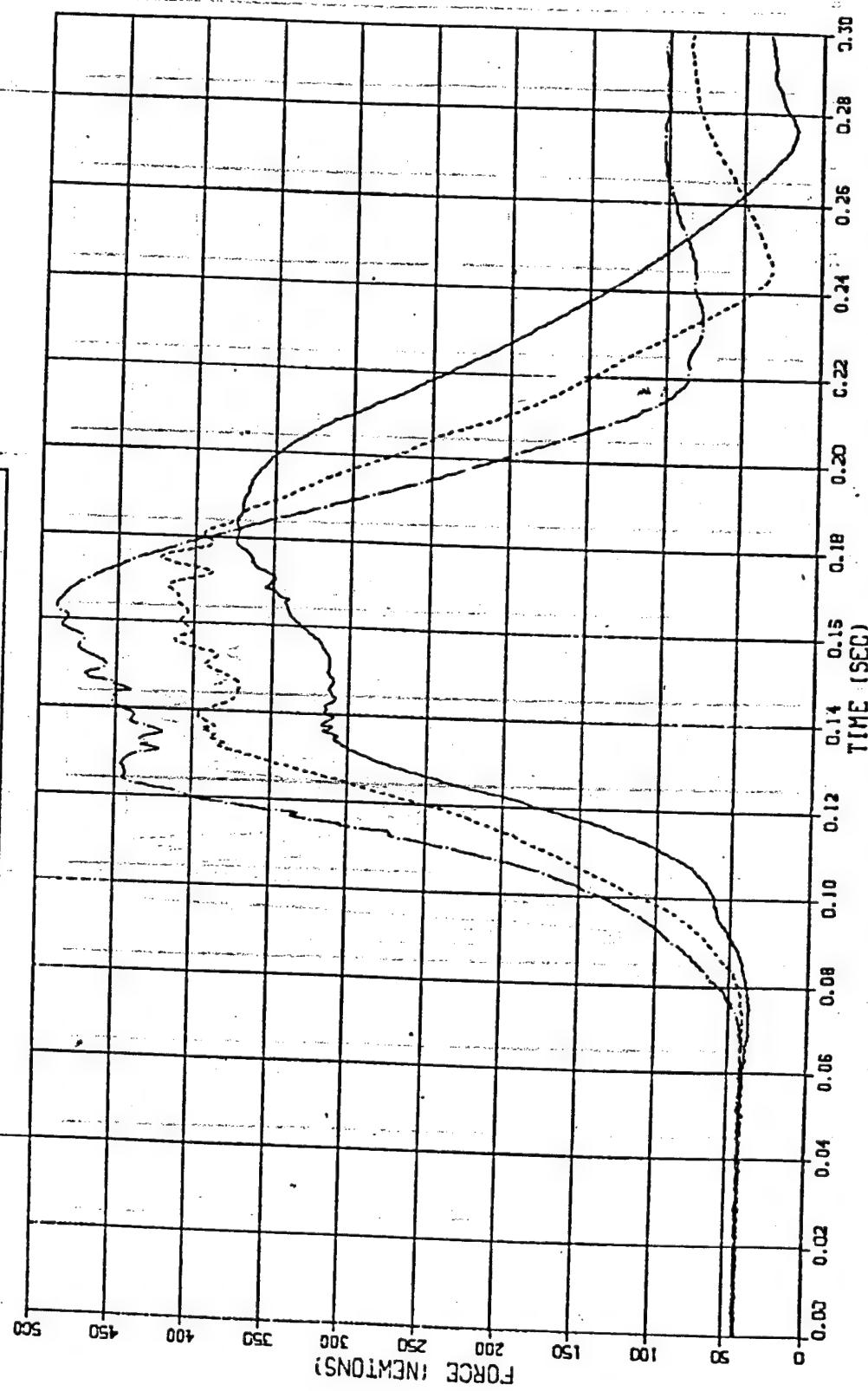


Fig 36

RESULTANT FORCE FOR MINUS X + PLUS Y SLED RUNS

LEGEND			
LX 4264 R.J.FORCE	HOD 34	0.270	
LX 4298 R.J.FORCE	HOD 34	0.136	
LX 4307 R.J.FORCE	HOD 34	0.446	

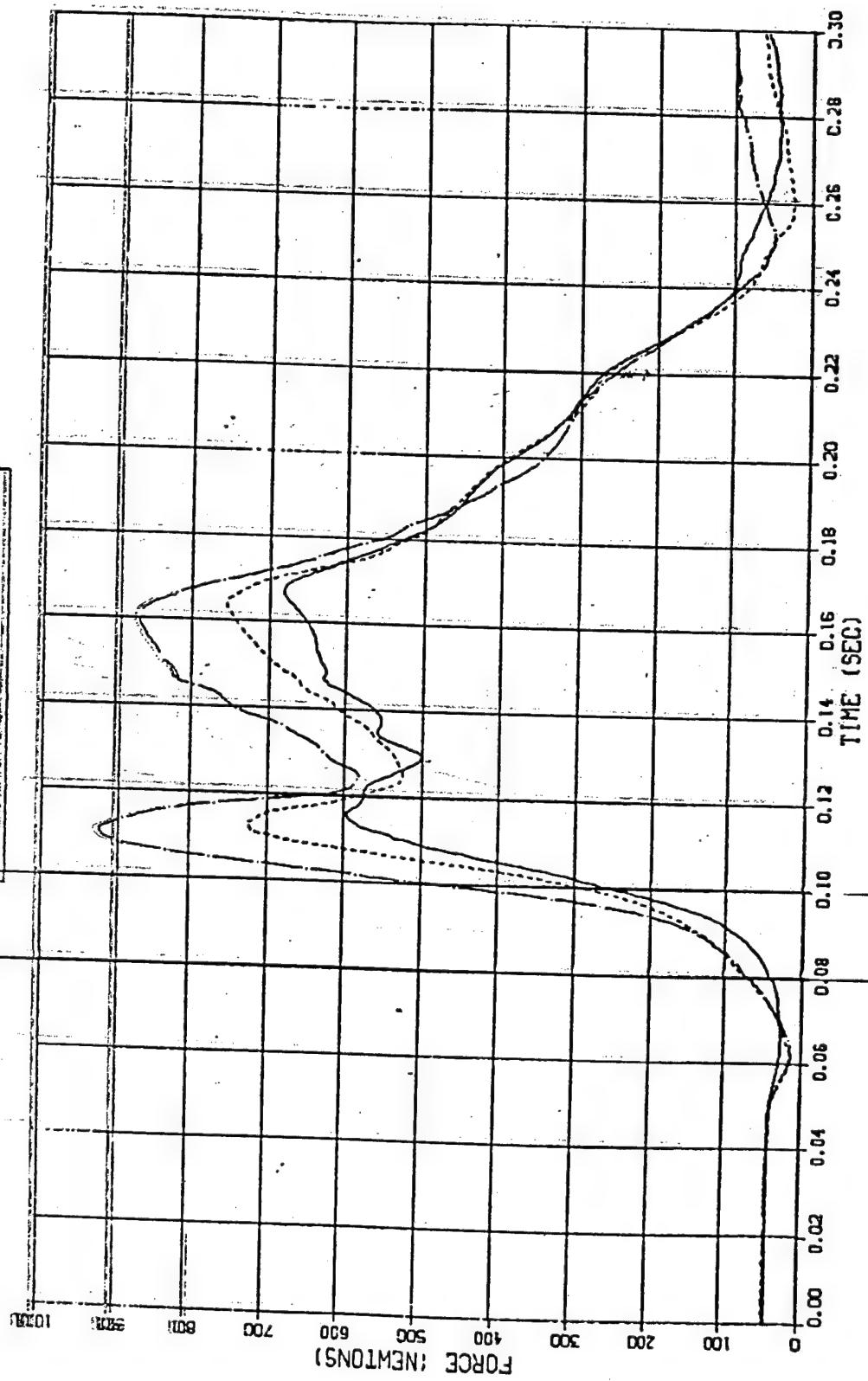


Fig 3C

**Figure 4. Resultant Torque Time-Courses Across -X, +Y and -X+Y
Vector Directions and Selected Accelerations For H134**



RESULTANT TORQUE FOR MINUS X SLED RUNS

LEGEND			
LX3693	RJTORD	H001	14.10.78
LX3961	RJTORD	H001	13.109.
LX3968	RJTORD	H001	14.316
LX3983	RJTORD	H001	15.586

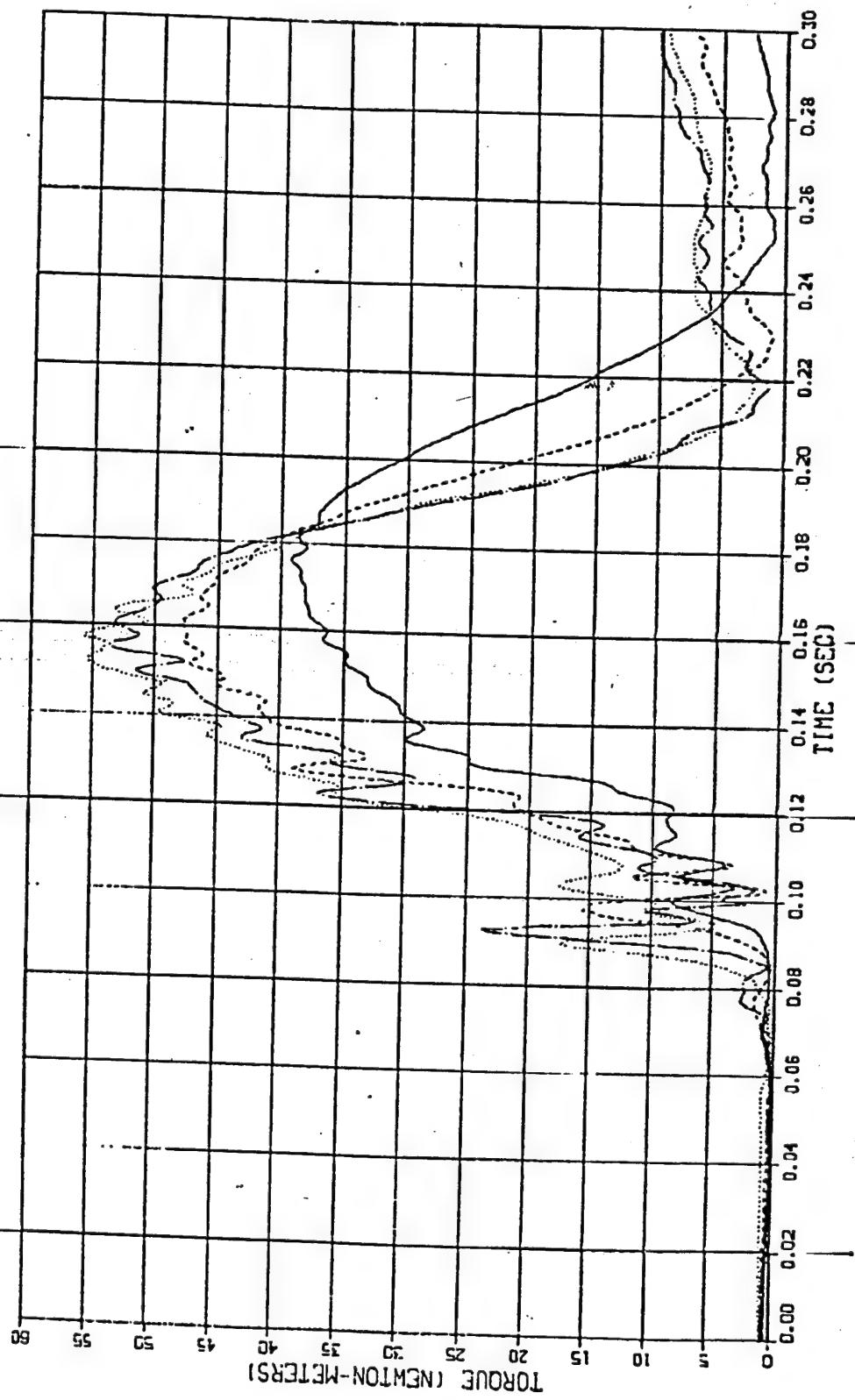


Fig 44

RESULTANT TORQUE FOR PLUS Y SLED RUNS

LEGEND			
LX4097	RJTORD	H00134	5.026
LX4112	RJTORD	H00134	6.116
LX4126	RJTORD	H00134	7.086

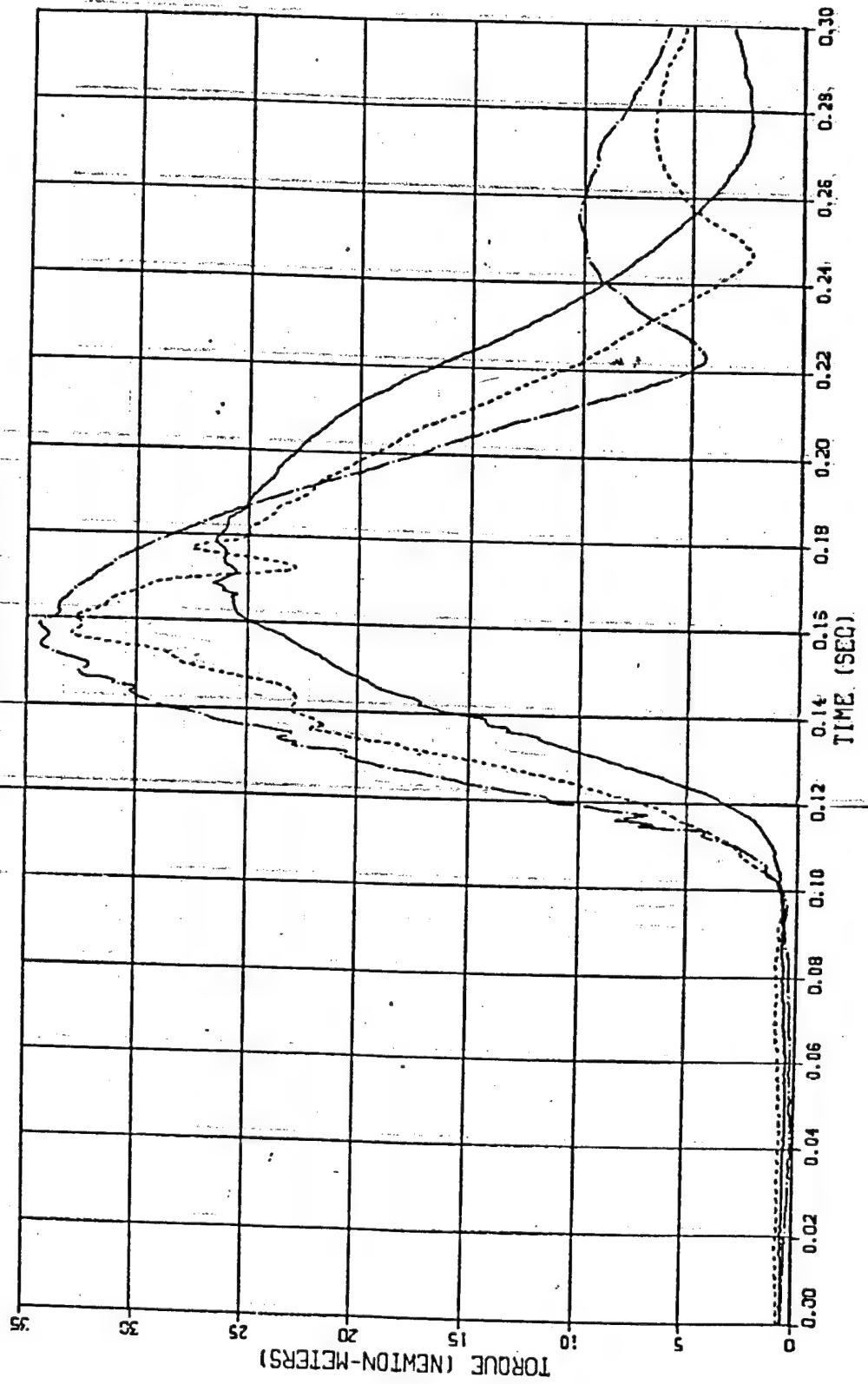


Fig 4b

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RESULTANT TORQUE FOR MINUS X + PLUS Y SLED RUNS

LEGEND	
LX1264 R JTGD	HD0134 9.276
LX1268 R JTGD	HD0131 10.136
LX1307 R JTGD	HD0134 11.416

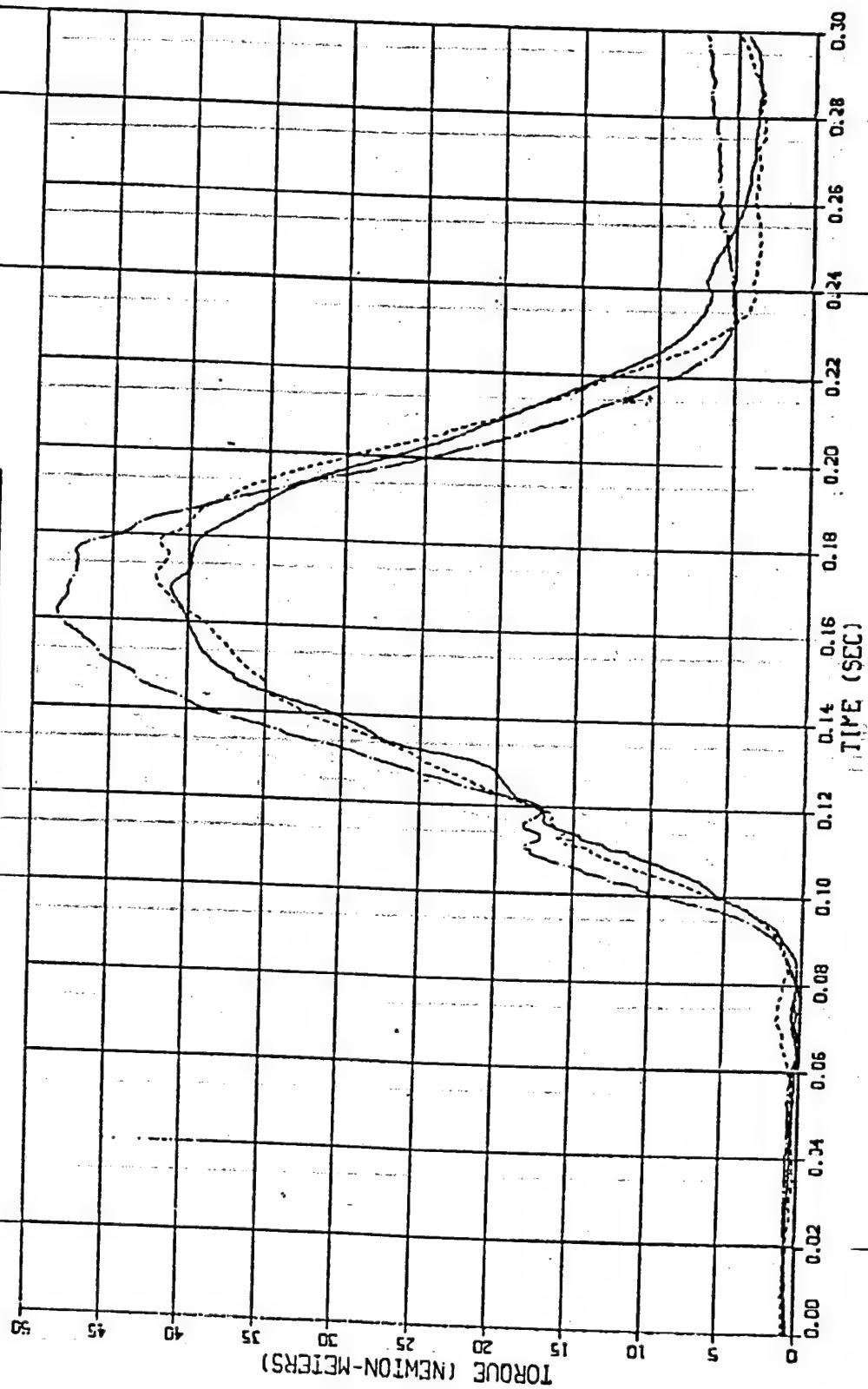


Fig 4C

**Figure 5. Head Injury Criteria (HIC) Time-Courses Across -X, +Y and -X+Y
Vector Directions and Selected Accelerations For H134.**



HEAD INJURY CRITERIA FOR MINUS X SLED RUNS

LEGEND			
LX3993	H1CAA	H00134	10.17G
LX3961	H1CAA	H00134	13.40G
LX3968	H1CAA	H00134	14.31G
LX3983	H1CAA	H00134	15.58G

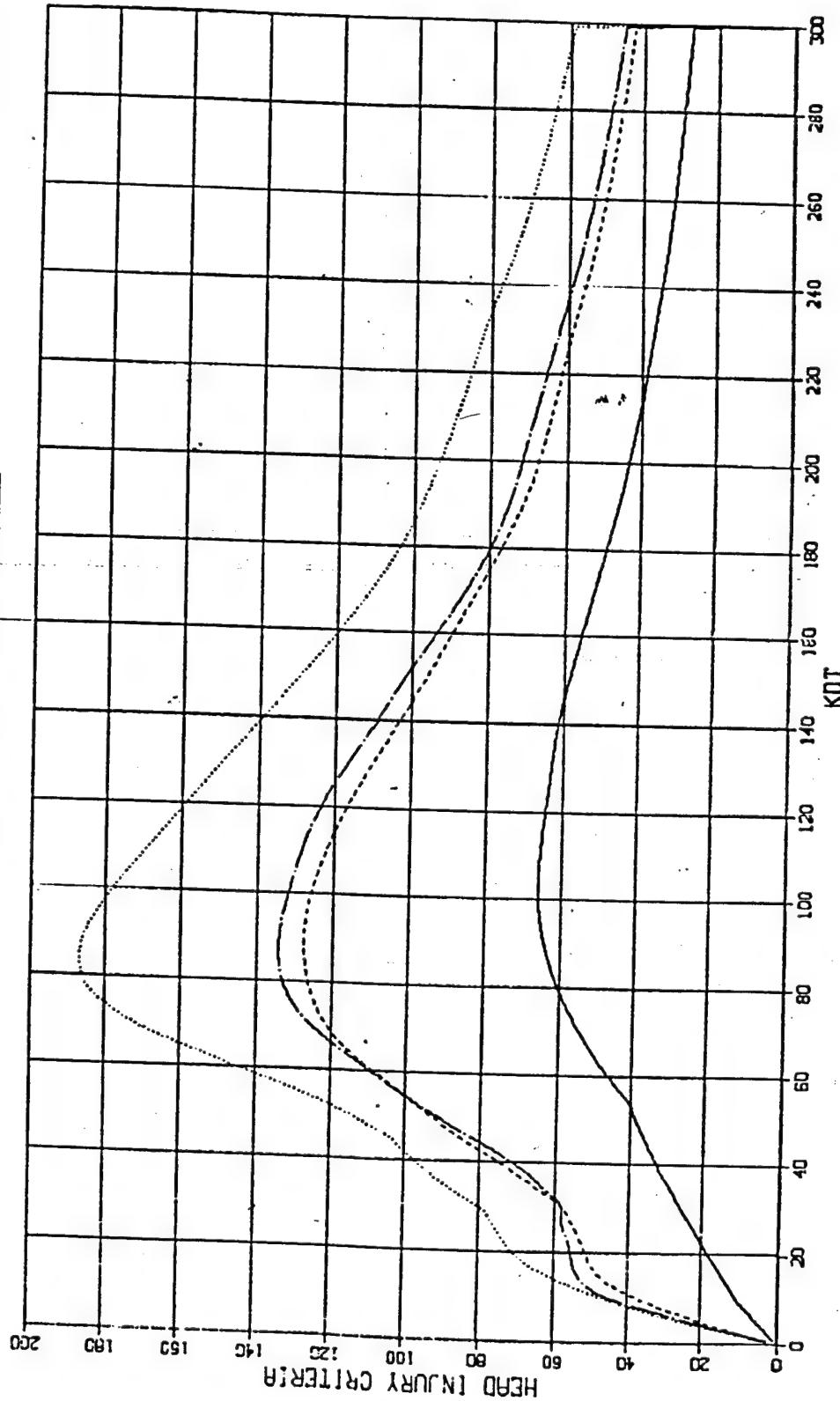


Fig 5a

HEAD INJURY CRITERIA FOR PLUS Y SLED RUNS

LEGEND		
LX4037	HICmax	H00134 5.02G
LX4112	HICmax	H00134 5.11G
LX4126	HICmax	H00134 7.08G

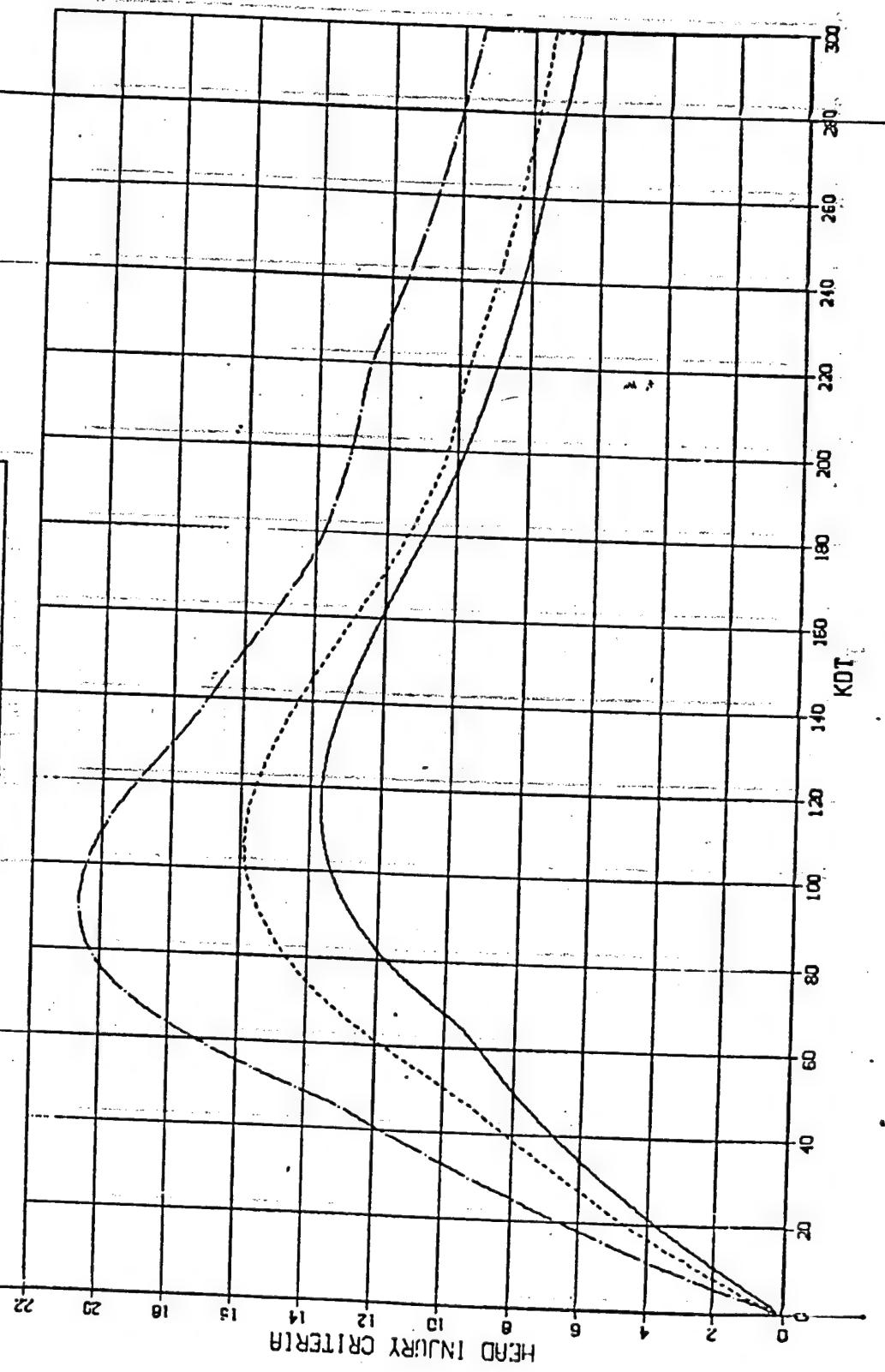


Fig 5b

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INJURY CRITERIA FOR MINUS X + PLUS Y SLED RUNS

LEGEND		
LX4264-H1000B	H00134	9.276
LX4288-H1000B	H00134	16.136
LX4307-H1000B	H00134	11.446

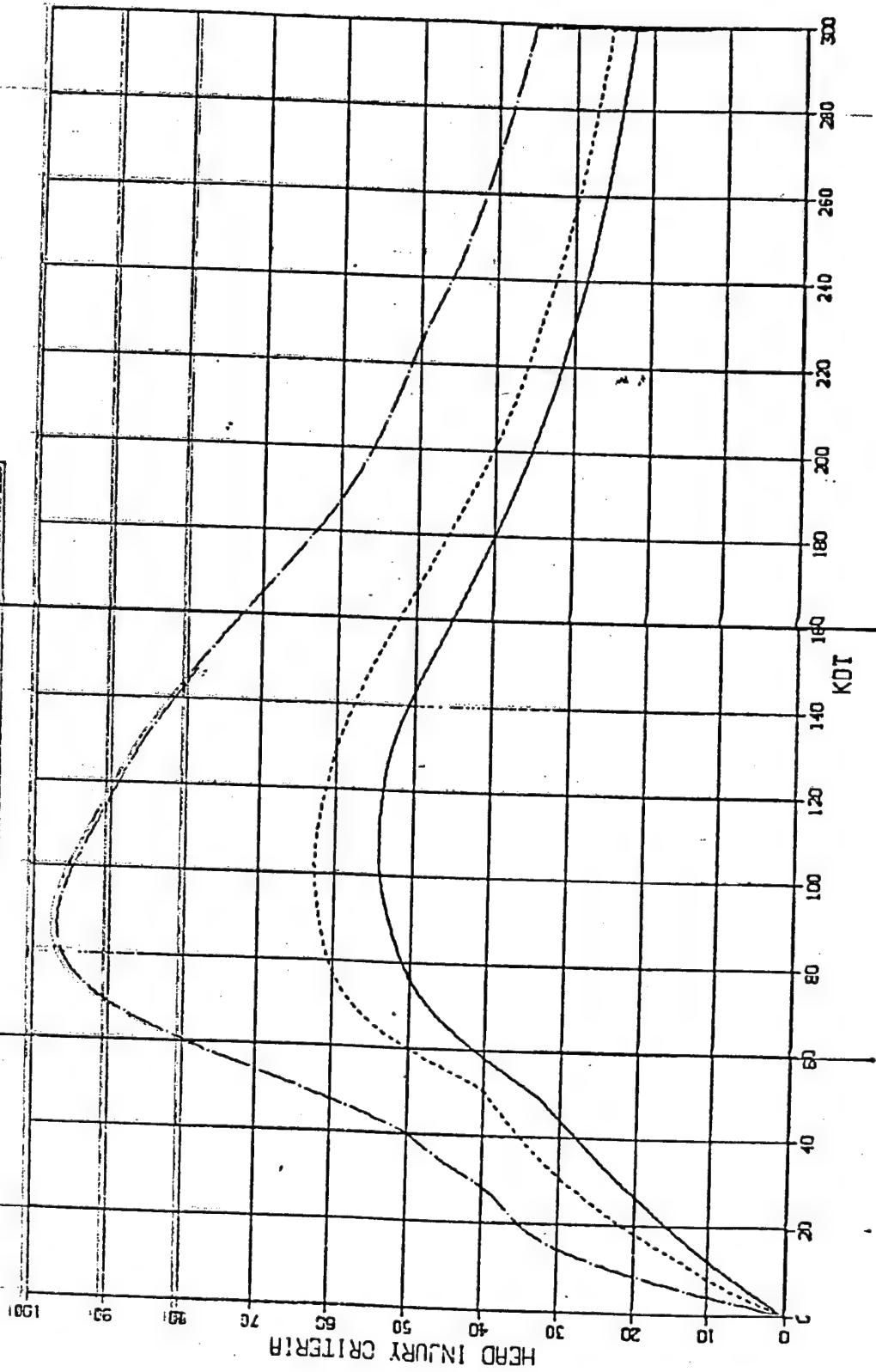


Fig 5C

Figure 6. Shear Force Time-Course Comparisons for Subjects with Large (H132) and Small (H135) Heads Across Selected -X, +Y, and -X+Y Impacts





SHEAR FORCE FOR MINUS X SLED DIRECTION

LEGEND
LX3982 SHFOREX_H00132 15.616
LX3970 SHFOREX_H00135 15.556

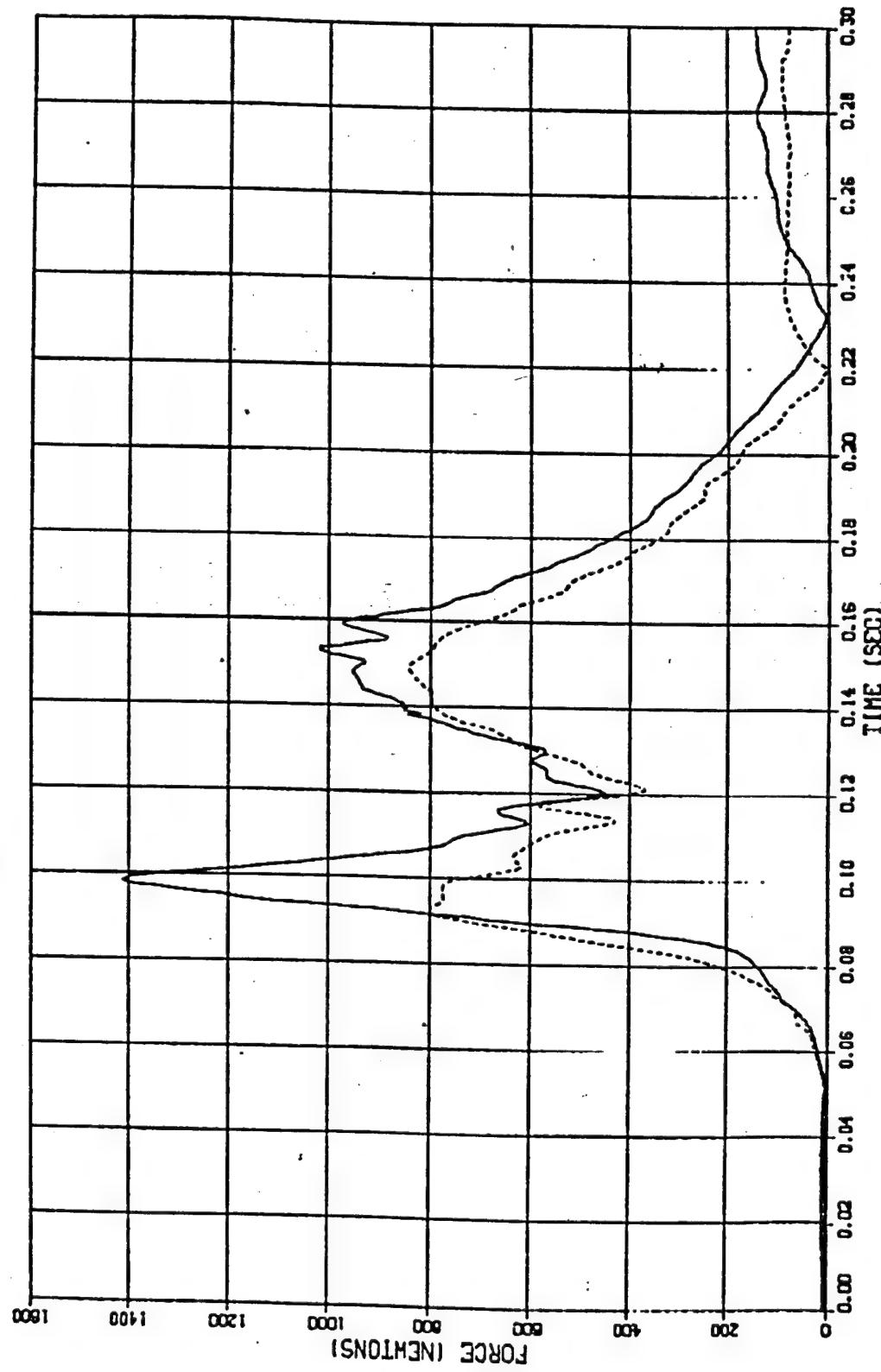


Fig 69



SHEAR FORCE FOR MINUS X : PLUS Y SLED RUNS

LEGEND
LX4297 SHFOREX H00132 10.036
LX4316 SHFOREX H00135 10.076

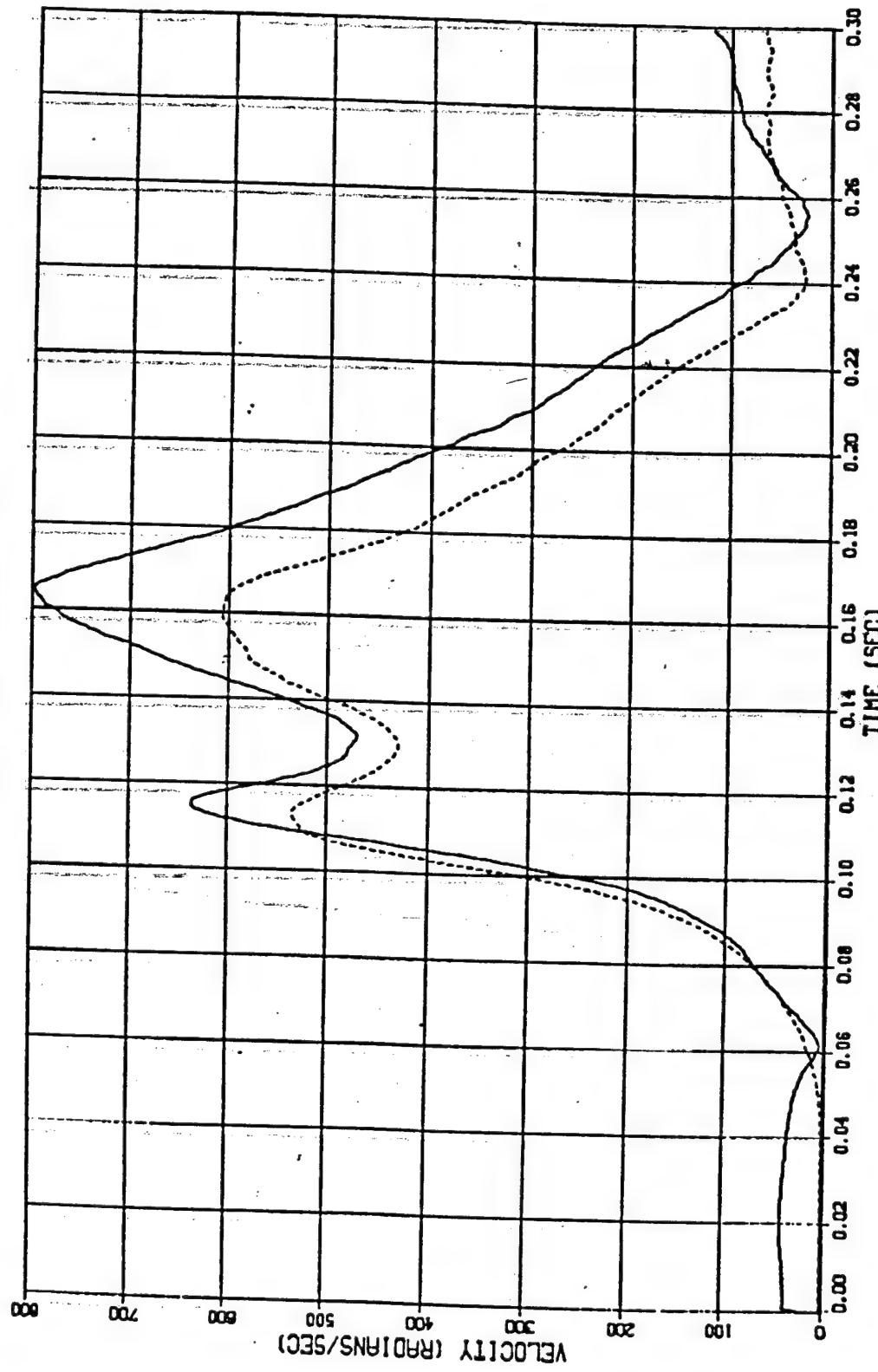


Fig 6c



Figure 7. Axial Force Time-Course Comparisons for Subjects with Large (H132) and Small (H135) Heads Across Selected -X, +Y and -X+Y Impacts





AXIAL FORCE FOR MINUS X SLED DIRECTION

LEGEND	
LX3982 FJCOXS	H00132 15,616
LX3920 FJCOXS	H00135 15,556

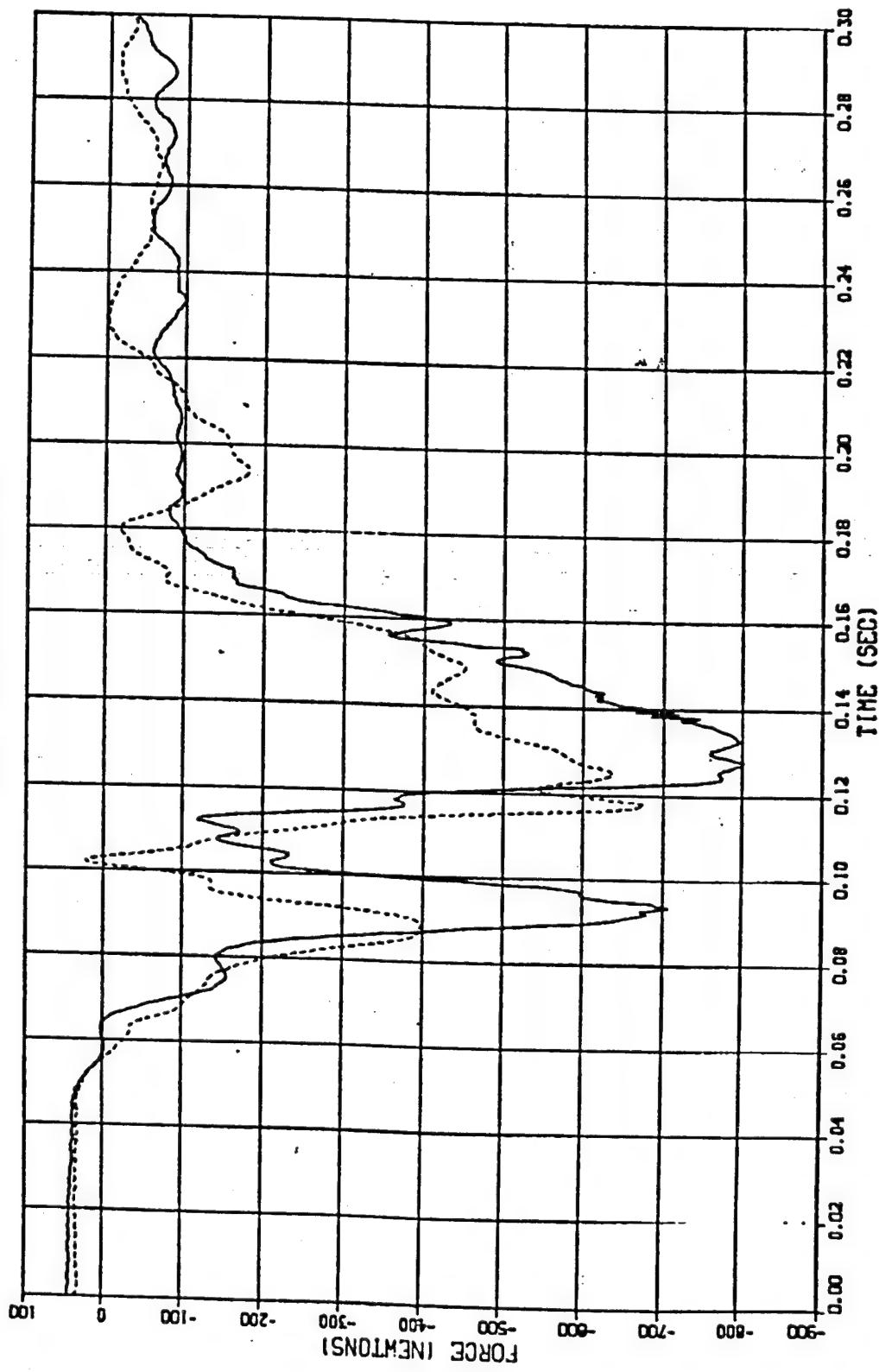


Fig - 701





AXIAL FORCE FOR PLUS Y SLED DIRECTION

LEGEND	
LX4128	FJCOXS H00132...Z.146
LX4131	FJCOXS H00135...Z.256..

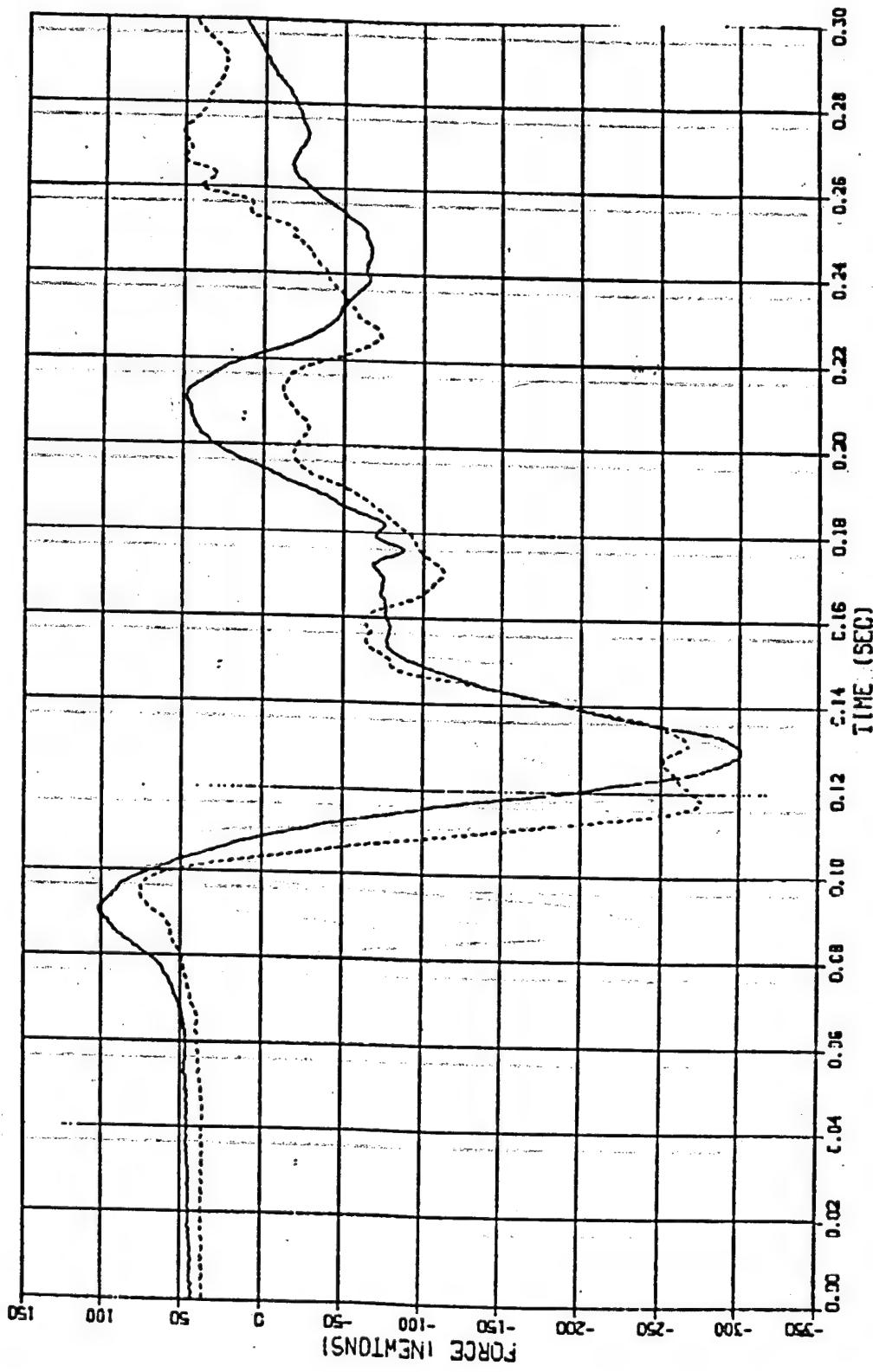


Fig 7b



4393
40018
AXIAL FORCE FOR MINUS X : PLUS Y SLED RUNS

LEGEND

LX4297 F JCOXS	H001332	10.036
LX4316 F JCOXS	H001335	10.076..

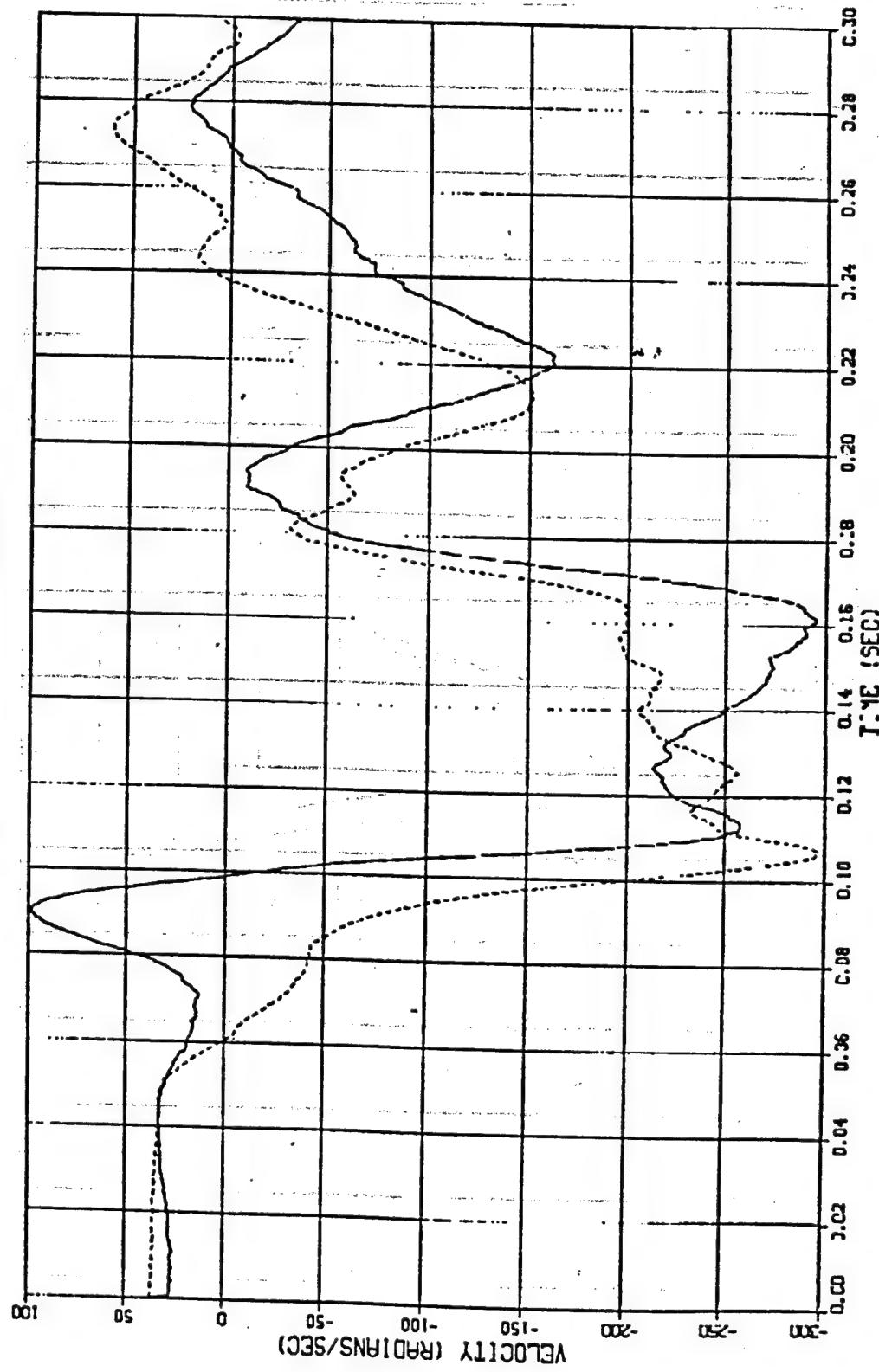


Fig 7c

AXIAL FORCE FOR MINUS X : PLUS Y SLED RUNS

LEGEND
LX4297 FJCOXS H00132 10.03G
LX4316 FJCOXS H00135 10.07G

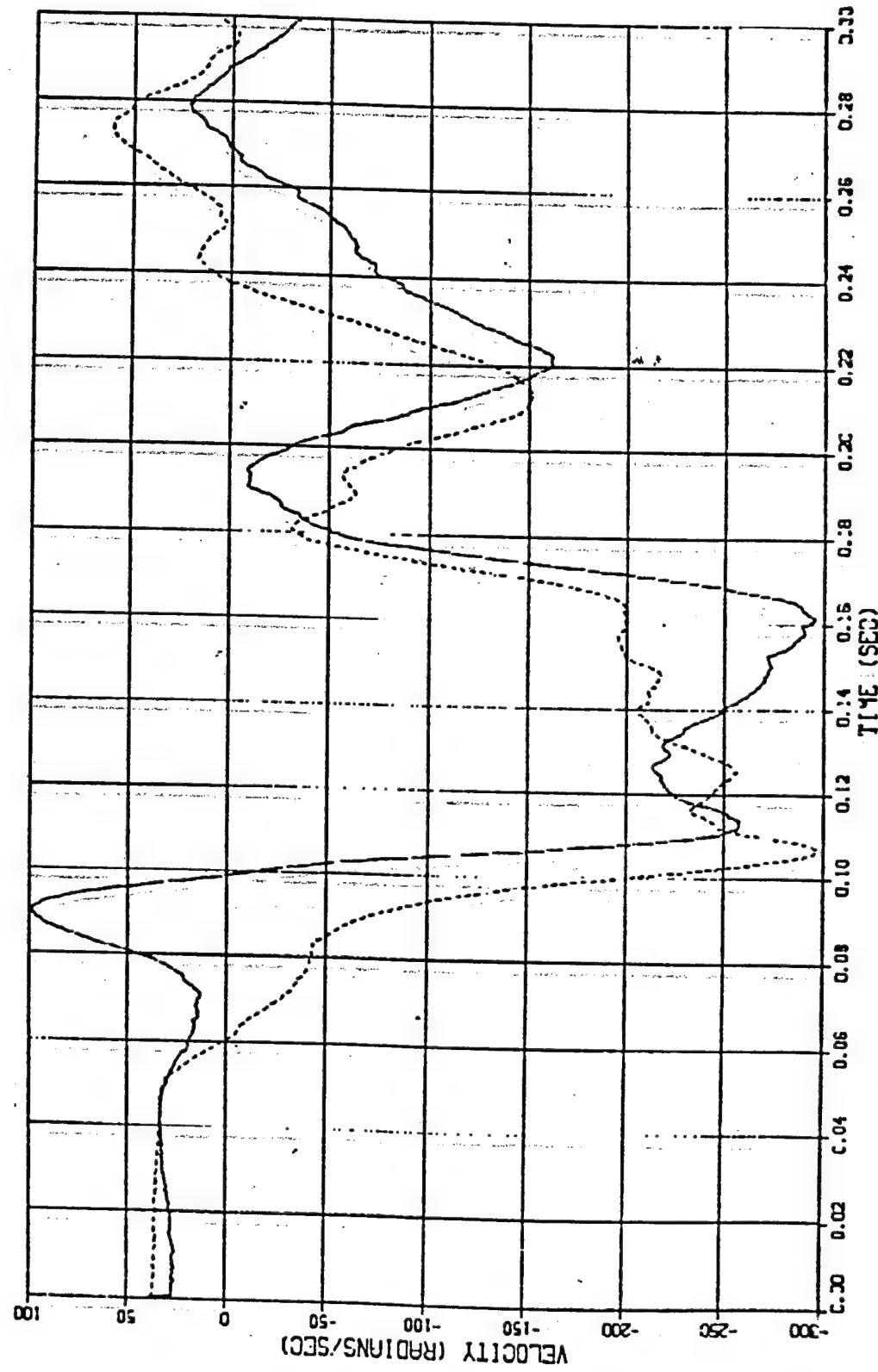


Figure 8. Resultant Torque Time-Course Comparisons for Subjects with Large (H132) and Small (H135) Heads Across -X, +Y and -X+Y Impacts



4393
CON-19
RESONANT TORQUE FOR MINUS X SLED RUNS

LEGEND
LX3982 RJTORO H00132 15.61G
LX3970 RJTORO H00135 15.55G

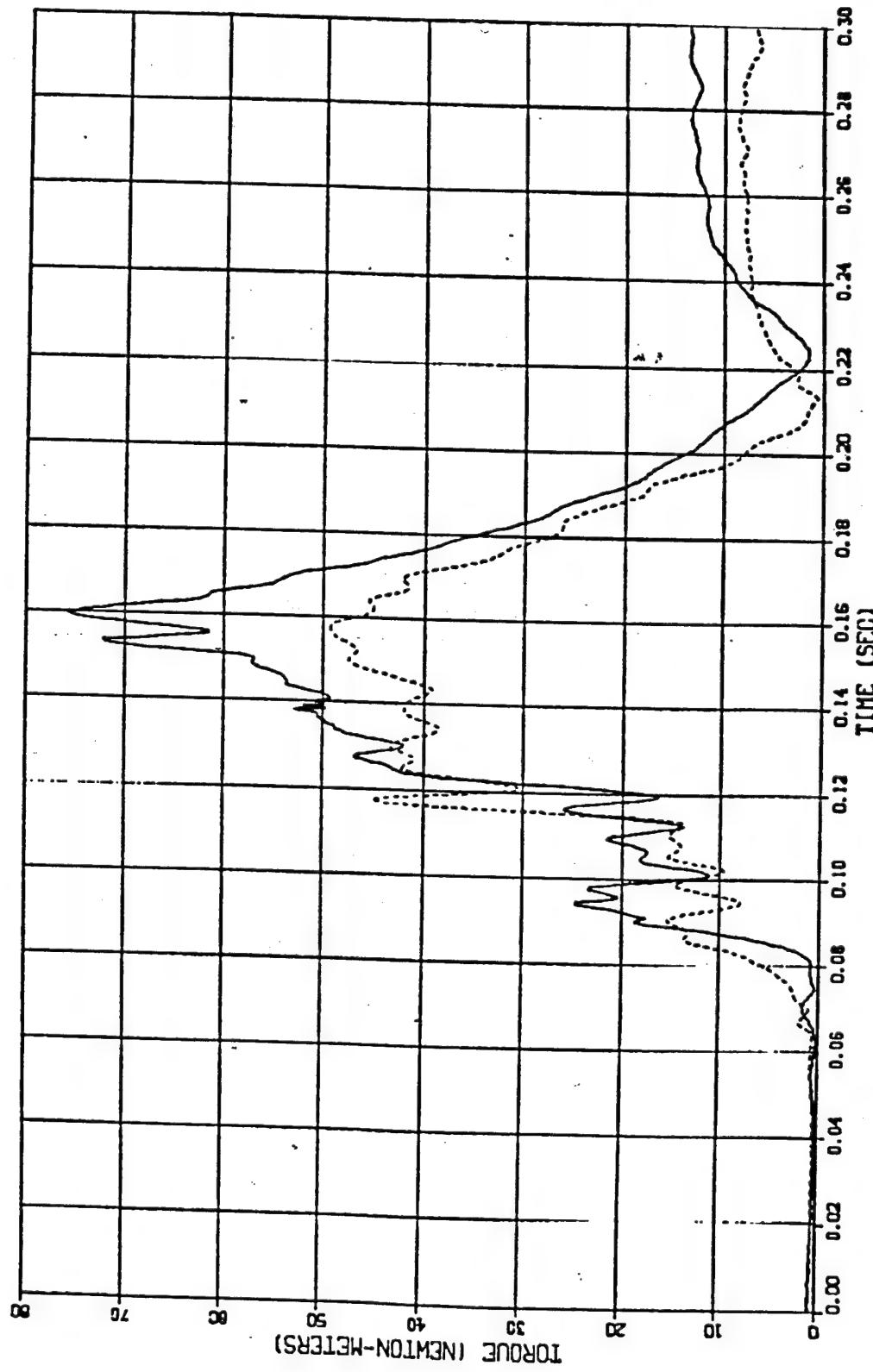


Fig. 84

4393
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RESULTANT TORQUE FOR PLUS Y SLED RUNS

LEGEND		
LX4128	RJT00	H00132 7.146
LX4131	RJT00	H00135 7.256

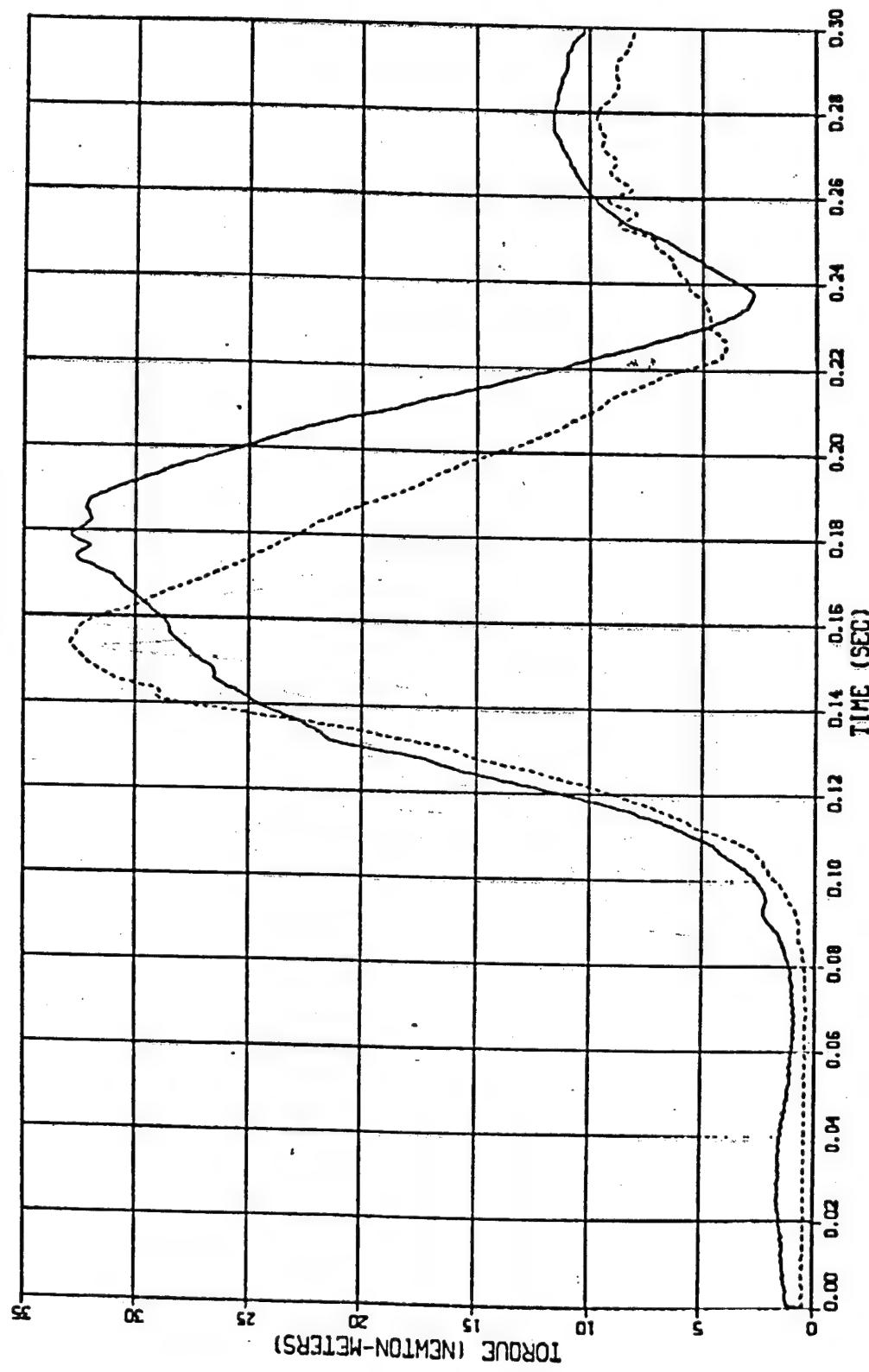
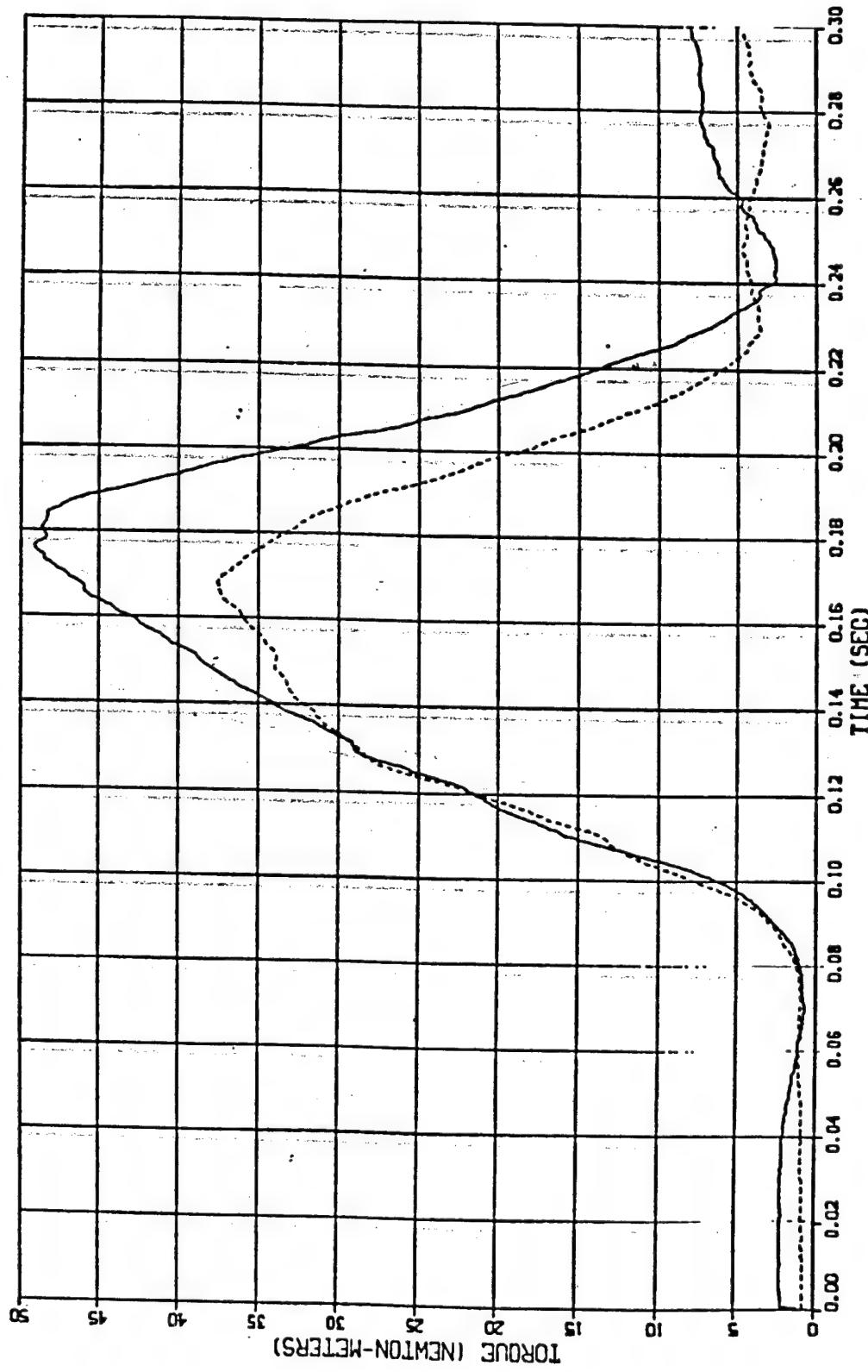


Fig 8b

4393
COPY 1
RESULTANT TORQUE FOR MINUS X : PLUS Y SLED RUNS

LEGEND
LX4297 RUTORO H00132 10.036
LX4316 RUTORO H00135 10.076



E. J. D.

APPENDIX

**SUBJECT (H131-H136) INJURY-RELATED VARIABLE SUMMARY TABLES FOR
SELECTED -X, +Y, AND -X+Y IMPACT ACCELERATIONS AT NBDL**



SUBJECT H00131

*** Head Anatomical Configuration ***

Head Mass : 4.449 Kg.

Head Center of Gravity: X = +0.0084 Y = -0.0006 Z = +0.0317 Meters

Head / Neck Center of Gravity: X = +0.0190 Y = +0.0000 Z = +0.5800 Meters

Eignvalues: 1 = +0.02198 2 = +0.02350 3 = +0.01529

Principal Axis Matrix	Moment of inertia matrix in A.C.S.
+0.82900 +0.00000 +0.55920	+0.019887 +0.000000 +0.003101
+0.00000 +1.00000 +0.00000	+0.000000 +0.023510 +0.000000
-0.55920 +0.00000 +0.82900	+0.003101 +0.000000 , +0.017381

*** Minus X Sled Runs ***

	10 G-Level	13 G-Level	14 G-Level	15 G-Level
Run	LX3908	LX3948	LX3987	LX3990
	Max	Min	Max	Min
Force X-Axis	140.59	-711.44	120.85	-828.81
Force Y-Axis	74.12	-76.47	26.99	77.77
Force Z-Axis	114.50	-404.53	44.34	-621.00
Force Result	788.51	4.63	980.34	15.66
			139.87-1058.48	127.16 -982.90
			56.72 -93.02	38.80 -131.41
			44.38 -721.15	45.03 -709.69
			1225.57	11.25
			1180.26	14.98

	10 G-Level	13 G-Level	14 G-Level	15 G-Level
Run	LX3993	LX3961	LX3968 87	LX3983 90 90
	Max	Min	Max	Min
Torque X-Axis	8.66	-6.95	6.70	-2.49
Torque Y-Axis	27.48	-45.81	11.48	-51.92
Torque Z-Axis	1.44	-2.96	0.89	-1.58
Torque Result	45.81	0.41	51.93	0.09
			7.56 -4.38	10.90 -3.77
			13.69 -58.89	13.10 -55.22
			3.28 -3.55	2.56 -2.71
			58.90 0.10	56.30 0.17

	10 G-Level	13 G-Level	14 G-Level	15 G-Level
Run	LX3993	LX3961	LX3968 87	LX3983 90 90✓
	HIC nbr	Width	HIC nbr	Width
HIC X-Axis	47.77	80.00	84.55	76.50
HIC Y-Axis	0.03	150.50	0.04	160.00
HIC Z-Axis	9.33	61.50	14.81	53.50
Resultant HIC	65.33	114.00	112.04	94.50
			114.03 75.00	112.08 74.50
			0.16 93.00	0.24 91.00
			19.79 47.50	21.08 44.00
			153.53 83.50	155.58 83.00

SUBJECT H00131
*** Plus Y Sled Runs ***

DOD

	5 G-Level		6 G-Level		6 G-Level		7 G-Level	
	Run LX4089	Run LX4109	Run LX4138	Run LX4124	Max	Min	Max	Min
Force X-Axis	43.83	-213.44	63.95	-218.45	58.88	-192.78	50.69	-190.52
Force Y-Axis	412.69	-46.53	400.74	-69.48	403.64	-73.89	403.69	-88.93
Force Z-Axis	54.85	-198.98	53.97	-309.86	75.07	-241.51	69.86	-323.39
Force Result	440.67	39.02	473.42	41.12	443.29	43.57	494.31	39.76

	5 G-Level		6 G-Level		6 G-Level		7 G-Level	
	Run LX4089	Run LX4109	Run LX4138	Run LX4124	Max	Min	Max	Min
Torque X-Axis	2.67	-32.58	4.32	-32.48	6.33	-35.00	7.09	-33.13
Torque Y-Axis	7.09	-11.98	7.10	-11.02	6.33	-11.24	8.92	-11.28
Torque Z-Axis	9.57	-1.86	11.70	-2.91	12.67	-3.13	12.95	-4.86
Torque Result	35.79	0.56	35.33	0.07	36.78	.71	35.41	0.25

	5 G-Level		6 G-Level		6 G-Level		7 G-Level	
	Run LX4089	Run LX4109	Run LX4138	Run LX4124	HIC nbr	Width	HIC nbr	Width
HIC X-Axis	11.95	94.00	12.65	94.00	10.85	97.50	13.02	84.50
HIC Y-Axis	0.24	129.00	0.20	130.00	0.52	73.00	0.41	68.00
HIC Z-Axis	1.19	59.50	2.59	64.00	3.18	67.00	2.66	60.00
Resultant HIC	15.28	95.00	17.85	101.50	16.92	107.50	18.09	94.00

*** Minus X / Plus Y ***

	7 G-Level		10 G-Level	
	Run LX4242	Run LX4251	Max	Min
Force X-Axis	6.81	-395.81	98.05	-700.19
Force Y-Axis	274.63	-2.14	394.24	-81.61
Force Z-Axis	51.17	-155.54	42.81	-467.41
Force Result	479.87	22.17	877.93	21.56

	7 G-Level		10 G-Level	
	Run LX4242	Run LX4251	Max	Min
Torque X-Axis	0.20	-20.71	6.91	-28.93
Torque Y-Axis	0.76	-27.23	7.37	-44.60
Torque Z-Axis	7.71	-2.34	12.52	-5.17
Torque Result	31.48	0.17	51.52	0.35

	7 G-Level		10 G-Level	
	Run LX4242	Run LX4251	HIC nbr	Width
HIC X-Axis	15.87	104.00	55.08	69.50
HIC Y-Axis	0.13	77.00	2.15	54.00
HIC Z-Axis	3.50	67.50	13.18	57.50
Resultant HIC	22.42	113.00	83.28	106.50

N8R



SUBJECT H00132

*** Head Anatomical Configuration ***

Head Mass : 4.523 Kg.

Head Center of Gravity: X = +0.0084 Y = -0.0006 Z = +0.0318 Meters

Head / Neck Center of Gravity: X = +0.0190 Y = +0.0000 Z = +0.5800 Meters

Eigenvalues: 1 = +0.02259 2 = +0.02415 3 = +0.01572

Principal Axis Matrix

+0.82900	+0.00000	+0.55920	Moment of inertia matrix in A.C.S.
+0.00000	+1.00000	+0.00000	+0.020440 +0.000000 +0.003185
-0.55920	+0.00000	+0.82900	+0.000000 +0.024150 +0.000000
			+0.003185 +0.000000 +0.017867

*** Minus X Sled Runs ***

	10 G-Level		13 G-Level		14 G-Level		15 G-Level	
	Run LX3989		Run LX3950		Run LX3957		Run LX3982	
	Max	Min	Max	Min	Max	Min	Max	Min
Force X-Axis	55.43	-691.57	118.72	-1535.00	110.60	-1199.90	143.99	-1395.33
Force Y-Axis	11.89	-88.28	64.71	-194.54	45.75	-177.12	23.92	-214.45
Force Z-Axis	80.33	-317.61	42.95	-983.66	44.89	-629.76	44.56	-801.69
Force Result	750.09	22.59	1823.22	4.61	1252.74	16.66	1514.52	8.89

	10 G-Level		13 G-Level		14 G-Level		15 G-Level	
	Run LX3989		Run LX3950		Run LX3957		Run LX3982	
	Max	Min	Max	Min	Max	Min	Max	Min
Torque X-Axis	6.39	-0.86	11.19	-15.49	7.80	-3.22	11.73	-6.22
Torque Y-Axis	4.54	-39.89	18.17	-68.34	11.66	-56.12	13.58	-75.11
Torque Z-Axis	0.62	-3.00	7.42	-4.79	2.59	-5.25	1.23	-4.15
Torque Result	40.37	0.10	68.58	0.11	56.59	0.34	75.71	0.11

	10 G-Level		13 G-Level		14 G-Level		15 G-Level	
	HIC nbr	Width	HIC nbr	Width	HIC nbr	Width	HIC nbr	Width
	Run LX3989		Run LX3950		Run LX3957		Run LX3982	
HIC X-Axis	40.62	81.50	93.49	72.50	118.32	74.50	112.06	65.00
HIC Y-Axis	0.02	184.00	0.24	187.00	0.11	212.00	0.08	66.50
HIC Z-Axis	6.25	75.50	16.61	19.50	13.42	41.00	29.03	41.00
Resultant HIC	50.01	94.50	126.49	83.50	146.99	81.00	167.47	83.00



SUBJECT H00132
 *** Plus Y Sled Runs ***

	5 G-Level		6 G-Level		7 G-Level	
	Run LX4090		Run LX4110		Run LX4128	
	Max	Min	Max	Min	Max	Min
Force X-Axis	42.26	-178.27	35.75	-315.75	60.02	-287.66
Force Y-Axis	291.58	-19.82	414.47	-89.96	392.60	-138.20
Force Z-Axis	77.41	-168.80	73.51	-320.10	101.81	-301.20
Force Result	343.08	38.09	539.94	28.51	495.36	44.30

	5 G-Level		6 G-Level		7 G-Level	
	Run LX4090		Run LX4110		Run LX4128	
	Max	Min	Max	Min	Max	Min
Torque X-Axis	1.92	-19.70	7.49	-29.34	10.84	-27.67
Torque Y-Axis	3.46	-8.27	5.56	-13.79	5.33	-15.05
Torque Z-Axis	8.00	-1.32	11.35	-2.96	13.85	-3.81
Torque Result	22.49	0.23	33.73	0.27	32.89	0.26

	5 G-Level		6 G-Level		7 G-Level	
	Run LX4090		Run LX4110		Run LX4128	
	HIC nbr	Width	HIC nbr	Width	HIC nbr	Width
HIC X-Axis	5.94	124.00	14.78	101.00	12.53	94.00
HIC Y-Axis	0.09	214.50	0.23	26.50	0.13	216.00
HIC Z-Axis	1.74	80.00	2.01	54.00	3.69	61.00
Resultant HIC	9.01	137.50	19.71	104.00	18.77	104.50

*** Minus X / Plus Y ***

	7 G-Level		10 G-Level		11 G-Level	
	Run LX4261		Run LX4297		Run LX4306	
	Max	Min	Max	Min	Max	Min
Force X-Axis	26.95	-568.61	64.44	-752.94	31.41	-713.83
Force Y-Axis	299.74	-60.54	311.01	-104.52	341.89	-74.08
Force Z-Axis	44.64	-202.31	98.66	-295.38	45.72	-301.87
Force Result	650.44	14.79	848.15	17.48	834.00	26.42

	7 G-Level		10 G-Level		11 G-Level	
	Max	Min	Max	Min	Max	Min
	Run LX4261		Run LX4297		Run LX4306	
Torque X-Axis	4.35	-20.38	6.62	-18.26	4.00	-21.82
Torque Y-Axis	2.03	-35.51	5.30	-45.39	3.26	-46.70
Torque Z-Axis	8.88	-1.31	10.91	-4.28	10.06	-2.59
Torque Result	40.70	0.46	49.07	0.52	51.65	0.62

	7 G-Level		10 G-Level		11 G-Level	
	Run LX4261		Run LX4297		Run LX4306	
	HIC nbr	Width	HIC nbr	Width	HIC nbr	Width
HIC X-Axis	36.62	103.50	45.65	77.00	50.09	84.00
HIC Y-Axis	0.46	44.00	1.22	32.50	0.57	28.00
HIC Z-Axis	3.15	56.50	7.04	53.50	8.83	53.00
Resultant HIC	45.72	108.50	60.14	95.00	66.50	95.50



SUBJECT H00133

*** Head Anatomical Configuration ***

Head Mass : 4.170 Kg.

Head Center of Gravity: X = +0.0082 Y = -0.0005 Z = +0.0310 Meters

Head / Neck Center of Gravity: X = +0.0190 Y = +0.0000 Z = +0.5800 Meters

Eignvalues: 1 = +0.01973 2 = +0.02110 3 = +0.01373

Principal Axis Matrix

+0.82900	+0.00000	+0.55920
+0.00000	+1.00000	+0.00000
-0.55920	+0.00000	+0.82900

Moment of inertia matrix in A.C.S.

+0.017853	+0.000000	+0.002781
+0.000000	+0.021100	+0.000000
+0.002781	+0.000000	+0.015605

*** Minus X Sled Runs ***

	10 G-Level	13 G-Level	14 G-Level	15 G-Level
Run LX3998	Run LX3951	Run LX3963	Run LX3986	
Max	Min	Max	Min	
Force X-Axis	96.70	-757.19	96.06	-855.84
Force Y-Axis	34.28	-78.60	70.55	-142.20
Force Z-Axis	40.77	-740.92	40.78	-726.01
Force Result	978.92	4.99	1122.77	11.35
			1147.43	10.67
				671.05
				2.96

	10 G-Level	13 G-Level	14 G-Level	15 G-Level
Run LX3998	Run LX3951	Run LX3963	Run LX3986	
Max	Min	Max	Min	
Torque X-Axis	9.22	-2.39	6.14	-4.61
Torque Y-Axis	3.14	-38.31	9.29	-48.99
Torque Z-Axis	1.34	-1.47	4.11	-3.40
Torque Result	39.15	0.15	49.06	0.03
			56.19	0.13
				39.15
				0.15

	10 G-Level	13 G-Level	14 G-Level	15 G-Level
Run LX3998	Run LX3951	Run LX3963	Run LX3986	
HIC nbr	Width	HIC nbr	Width	
HIC X-Axis	43.28	97.00	86.99	76.50
HIC Y-Axis	0.06	73.00	0.06	216.00
HIC Z-Axis	5.11	62.50	17.29	48.00
Resultant HIC	55.32	106.50	120.17	94.00
			125.77	89.00
				177.62
				88.50



SUBJECT H00133
 *** Plus Y Sled Runs ***

	5 G-Level		6 G-Level		7 G-Level	
	Run LX4093		Run LX4111		Run LX4125	
	Max	Min	Max	Min	Max	Min
Force X-Axis	43.51	-163.40	27.00	-188.44	24.50	-274.48
Force Y-Axis	364.71	-34.23	395.26	-51.60	577.36	-108.84
Force Z-Axis	47.67	-159.00	71.89	-276.20	68.77	-369.02
Force Result	380.65	40.25	444.90	30.88	647.16	36.46

	5 G-Level		6 G-Level		7 G-Level	
	Run LX4093		Run LX4111		Run LX4125	
	Max	Min	Max	Min	Max	Min
Torque X-Axis	2.84	-28.16	3.91	-33.20	8.71	-44.60
Torque Y-Axis	4.70	-10.12	3.30	-9.25	4.26	-12.65
Torque Z-Axis	9.38	-0.27	10.32	-1.15	16.68	-2.43
Torque Result	30.38	0.49	35.42	0.69	49.05	0.64

	5 G-Level		6 G-Level		7 G-Level	
	Run LX4093		Run LX4111		Run LX4125	
	HIC nbr	Width	HIC nbr	Width	HIC nbr	Width
HIC X-Axis	11.62	104.50	16.36	97.00	24.85	74.00
HIC Y-Axis	0.18	148.50	0.25	135.00	0.23	79.50
HIC Z-Axis	0.63	268.00	1.72	61.50	3.95	44.00
Resultant HIC	13.74	106.00	21.05	102.50	32.93	78.50

*** Minus X / Plus Y ***

	7 G-Level		10 G-Level	
	Run LX4236		Run LX4240	
	Max	Min	Max	Min
Force X-Axis	3.74	-343.93	11.38	-447.93
Force Y-Axis	338.00	-8.19	499.11	-39.79
Force Z-Axis	45.92	-159.02	52.51	-273.00
Force Result	497.62	213.34	643.11	12.44

	7 G-Level		10 G-Level	
	Run LX4236		Run LX4240	
	Max	Min	Max	Min
Torque X-Axis	1.84	-22.29	2.80	-26.65
Torque Y-Axis	0.34	-20.87	0.80	-25.14
Torque Z-Axis	9.18	-0.11	11.45	-0.94
Torque Result	31.33	0.09	36.51	0.22

	7 G-Level		10 G-Level	
	Run LX4236		Run LX4240	
	HIC nbr	Width	HIC nbr	Width
HIC X-Axis	26.26	107.50	39.86	104.50
HIC Y-Axis	0.18	45.50	0.33	44.50
HIC Z-Axis	1.04	115.00	3.98	57.50
Resultant HIC	29.97	108.50	50.50	106.50



SUBJECT H00134

*** Head Anatomical Configuration ***

Head Mass : 4.278 Kg.

Head Center of Gravity: X = +0.0083 Y = -0.0005 Z = +0.0313 Meters

Head / Neck Center of Gravity: X = +0.0190 Y = +0.0000 Z = +0.5800 Meters

Eigenvalues: 1 = +0.02059 2 = +0.02201 3 = +0.01433

Principal Axis Matrix

+0.82900	+0.00000	+0.55920
+0.00000	+1.00000	+0.00000
-0.55920	+0.00000	+0.82900

Moment of inertia matrix in A.C.S.

+0.018631	+0.000000	+0.002902
+0.000000	+0.022010	+0.000000
+0.002902	+0.000000	+0.016287

*** Minus X Sled Runs ***

10 G-Level		13 G-Level		14 G-Level		15 G-Level	
Run LX3993		Run LX3961		Run LX3968		Run LX3983	
Max	Min	Max	Min	Max	Min	Max	Min

Force X-Axis	28.56	-629.12	81.13	-969.39	92.79	-961.99	100.82	-994.27
Force Y-Axis	20.05	-42.76	30.54	-84.36	57.22	-119.35	67.90	-89.18
Force Z-Axis	46.41	-418.24	41.61	-739.49	43.32	-826.82	42.62	-769.25
Force Result	722.41	14.38	1089.09	+11.57	1114.39	13.86	1182.19	10.44

10 G-Level		13 G-Level		14 G-Level		15 G-Level	
Run LX3993		Run LX3961		Run LX3968		Run LX3983	
Max	Min	Max	Min	Max	Min	Max	Min

Torque X-Axis	3.77	-1.98	5.67	-1.91	7.27	-5.35	7.75	-3.02
Torque Y-Axis	2.06	-39.14	7.09	-47.83	10.04	-53.65	9.23	-55.22
Torque Z-Axis	0.63	-0.68	1.50	-2.65	2.39	-4.18	1.05	-1.71
Torque Result	39.25	+0.05	47.99	+0.05	53.72	+0.02	55.76	0.15

10 G-Level		13 G-Level		14 G-Level		15 G-Level	
Run LX3993		Run LX3961		Run LX3968		Run LX3983	
HIC Nbr	Width						

HIC X-Axis	46.27	80.00	96.30	67.50	93.33	67.00	137.66	71.50
HIC Y-Axis	0.08	89.00	0.64	200.50	0.11	121.00	0.22	175.00
HIC Z-Axis	10.54	65.00	18.36	54.50	25.43	49.50	25.01	43.00
Resultant HIC	66.03	103.00	127.56	89.00	134.16	87.00	186.80	84.00



SUBJECT H00134
 *** Plus Y Sled Runs ***

	5 G-Level		6 G-Level		7 G-Level	
	Run LX4097		Run LX4112		Run LX4126	
	Max	Min	Max	Min	Max	Min
Force X-Axis	20.59	-171.14	31.85	-243.86	60.02	-262.26
Force Y-Axis	330.00	-42.60	366.24	-67.13	399.14	-87.26
Force Z-Axis	43.97	-162.33	52.70	-250.91	47.34	-307.52
Force Result	374.40	+16.35	422.86	+31.73	489.36	+41.01

	5 G-Level		6 G-Level		7 G-Level	
	Run LX4097		Run LX4112		Run LX4126	
	Max	Min	Max	Min	Max	Min
Torque X-Axis	2.77	-24.35	5.53	-31.37	6.92	-31.04
Torque Y-Axis	2.25	-10.17	4.14	-14.51	8.02	-14.86
Torque Z-Axis	7.90	-0.25	10.94	-2.23	10.66	-2.81
Torque Result	26.57	+0.34	33.02	+0.45	34.45	+0.04

	5 G-Level		6 G-Level		7 G-Level	
	Run LX4097		Run LX4112		Run LX4126	
	HIC Nbr	Width	HIC Nbr	Width	HIC Nbr	Width
HIC X-Axis	11.15	114.50	13.69	103.50	16.27	86.50
HIC Y-Axis	0.08	133.00	0.06	143.50	0.21	112.00
HIC Z-Axis	1.14	70.00	0.98	69.50	2.08	55.00
Resultant HIC	13.70	116.50	15.89	105.50	20.62	91.00

*** Minus X / Plus Y ***

	9 G-Level		10 G-Level		11 G-Level	
	Run LX4264		Run LX4298		Run LX4307	
	Max	Min	Max	Min	Max	Min
Force X-Axis	30.28	-520.00	37.18	-589.15	43.68	-680.55
Force Y-Axis	356.98	-48.65	341.57	-49.29	361.52	-86.75
Force Z-Axis	42.31	-337.14	43.75	-473.28	42.29	-631.21
Force Result	681.84	25.56	755.83	+14.07	924.77	12.78

	9 G-Level		10 G-Level		11 G-Level	
	Run LX4264		Run LX4298		Run LX4307	
	Max	Min	Max	Min	Max	Min
Torque X-Axis	4.33	-28.12	3.69	-23.99	6.58	-29.66
Torque Y-Axis	2.47	-32.52	3.15	-36.92	3.69	-42.53
Torque Z-Axis	10.54	-0.90	10.82	-1.49	12.12	-0.88
Torque Result	41.17	+0.06	42.17	+0.17	48.55	+0.03

	9 G-Level		10 G-Level		11 G-Level	
	Run LX4264		Run LX4298		Run LX4307	
	HIC Nbr	Width	HIC Nbr	Width	HIC Nbr	Width
HIC X-Axis	40.91	82.50	45.56	74.50	70.22	75.00
HIC Y-Axis	0.35	188.00	0.23	142.00	0.66	196.00
HIC Z-Axis	5.30	114.00	8.85	63.00	12.53	105.50
Resultant HIC	54.40	107.00	62.68	102.00	96.89	87.00



SUBJECT H00135

*** Head Anatomical Configuration ***

Head Mass : 3.791 Kg.
 Head Center of Gravity: X = +0.0080 Y = -0.0005 Z = +0.0300 Meters
 Head / Neck Center of Gravity: X = +0.0190 Y = +0.0000 Z = +0.5800 Meters
 Eigenvalues: 1 = +0.01683 2 = +0.01800 3 = +0.01171

Principal Axis Matrix			Moment of inertia matrix in A.C.S.		
+0.82900	+0.00000	+0.55920	+0.015228	+0.000000	+0.002374
+0.00000	+1.00000	+0.00000	+0.000000	+0.018000	+0.000000
-0.55920	+0.00000	+0.82900	+0.002374	+0.000000	+0.013310

*** Minus X Sled Runs ***

	10 G-Level		13 G-Level		14 G-Level		15 G-Level	
	Run LX3916		Run LX3955		Run LX3965		Run LX3970	
	Max	Min	Max	Min	Max	Min	Max	Min
Force X-Axis	80.70	-632.31	122.75	-786.30	114.80	-1078.20	91.83	-840.30
Force Y-Axis	36.37	-109.08	25.83	-120.50	44.89	-141.20	16.60	-210.44
Force Z-Axis	71.48	-360.26	114.49	-559.82	192.81	-764.17	36.55	-675.56
Force Result	717.10	6.56	891.40	10.25	1294.03	11.38	955.28	9.40

	10 G-Level		13 G-Level		14 G-Level		15 G-Level	
	Run LX3916		Run LX3955		Run LX3965		Run LX3970	
	Max	Min	Max	Min	Max	Min	Max	Min
Torque X-Axis	8.27	-2.39	9.50	-2.26	9.68	-5.45	18.09	-1.70
Torque Y-Axis	5.41	-33.14	7.63	-44.79	8.78	-68.54	8.68	-49.17
Torque Z-Axis	0.94	-1.29	2.52	-2.94	3.68	-3.70	2.05	-4.10
Torque Result	33.21	0.13	44.82	0.24	68.58	0.17	49.35	0.27

	10 G-Level		13 G-Level		14 G-Level		15 G-Level	
	Run LX3916		Run LX3955		Run LX3965		Run LX3970	
	HIC Nbr	Width						
HIC X-Axis	50.13	85.50	90.27	75.50	116.77	74.00	109.17	75.50
HIC Y-Axis	0.08	38.50	0.06	200.00	0.24	207.00	0.06	229.00
HIC Z-Axis	9.27	137.00	16.62	49.50	23.61	108.50	24.95	45.00
Resultant HIC	66.22	107.50	120.46	87.50	162.35	84.00	154.17	86.50



SUBJECT H00135
 *** Plus Y Sled Runs ***

	5 G-Level		6 G-Level		7 G-Level	
	Run LX4095		Run LX4114		Run LX4131	
	Max	Min	Max	Min	Max	Min
Force X-Axis	31.37	-144.94	30.70	-204.51	52.96	-254.57
Force Y-Axis	286.25	-61.93	329.41	-91.10	365.60	-120.51
Force Z-Axis	54.27	-140.82	63.02	-224.09	76.10	-275.73
Force Result	325.10	30.09	375.44	32.69	447.19	36.17

	5 G-Level		6 G-Level		7 G-Level	
	Run LX4095		Run LX4114		Run LX4131	
	Max	Min	Max	Min	Max	Min
Torque X-Axis	5.34	-21.65	6.21	-23.75	8.84	-28.43
Torque Y-Axis	3.07	-8.76	3.55	-9.52	7.36	-12.95
Torque Z-Axis	7.75	-1.17	7.91	-1.94	10.66	-3.03
Torque Result	23.96	0.23	26.48	0.27	32.92	0.33

	5 G-Level		6 G-Level		7 G-Level	
	Run LX4095		Run LX4114		Run LX4131	
	HIC Nbr	Width	HIC Nbr	Width	HIC Nbr	Width
HIC X-Axis	11.42	117.00	14.85	102.50	40.85	81.00
HIC Y-Axis	0.13	151.50	0.15	141.50	0.32	131.50
HIC Z-Axis	0.89	74.00	1.30	48.50	3.88	54.50
Resultant HIC	13.77	121.00	18.28	102.00	50.76	101.00

*** Minus X / Plus Y ***

	9 G-Level		10 G-Level	
	Run LX4314		Run LX4316	
	Max	Min	Max	Min
Force X-Axis
Force Y-Axis
Force Z-Axis
Force Result

	9 G-Level		10 G-Level	
	Run LX4314		Run LX4316	
	Max	Min	Max	Min
Torque X-Axis
Torque Y-Axis
Torque Z-Axis
Torque Result

	9 G-Level		10 G-Level	
	Run LX4314		Run LX4316	
	HIC Nbr	Width	HIC Nbr	Width
HIC X-Axis	40.85	81.00	51.32	79.00
HIC Y-Axis	0.32	131.00	0.37	162.00
HIC Z-Axis	3.88	54.50	6.10	55.50
Resultant HIC	50.76	101.50	63.92	94.00



SUBJECT H00136

*** Head Anatomical Configuration ***

Head Mass : 4.235 Kg.

Head Center of Gravity: X = +0.0083 Y = -0.0005 Z = +0.0312 Meters

Head / Neck Center of Gravity: X = +0.0190 Y = +0.0000 Z = +0.5800 Meters

Eignvalues: 1 = +0.02024 2 = +0.02164 3 = +0.01409

Principal Axis Matrix

+0.82900	+0.00000	+0.55920
+0.00000	+1.00000	+0.00000
-0.55920	+0.00000	+0.82900

Moment of inertia matrix in A.C.S.

+0.018316	+0.000000	+0.002851
+0.000000	+0.021640	+0.000000
+0.002851	+0.000000	+0.016012

*** Minus X Sled Runs ***

	10 G-Level		12 G-Level		13 G-Level		14 G-Level	
	Run LX3918		Run LX3942		Run LX3953		Run LX3962	
	Max	Min	Max	Min	Max	Min	Max	Min

Force X-Axis
Force Y-Axis
Force Z-Axis
Force Result

	10 G-Level		12 G-Level		13 G-Level		14 G-Level	
	Run LX3918		Run LX3942		Run LX3953		Run LX3962	
	Max	Min	Max	Min	Max	Min	Max	Min

Torque X-Axis
Torque Y-Axis
Torque Z-Axis
Torque Result

	10 G-Level		12 G-Level		13 G-Level		14 G-Level	
	Run LX3918		Run LX3942		Run LX3953		Run LX3962	
	HIC Nbr	Width						
HIC X-Axis	48.48	91.50	65.83	92.50	85.96	83.50	99.13	85.50
HIC Y-Axis	0.08	528.50	0.18	189.50	0.18	194.00	0.09	84.00
HIC Z-Axis	8.95	61.00	16.22	53.50	19.11	52.00	14.07	120.00
Resultant HIC	65.84	107.50	95.49	95.50	121.16	100.00	128.32	85.50



SUBJECT H00136

*** Plus Y Sled Runs ***

	5 G-Level	6 G-Level	7 G-Level			
Run	LX4098	LX4142	LX4153			
	Max	Min	Max	Min	Max	Min
HIC X-Axis	9.42	118.00	13.37	100.00	18.48	82.00
HIC Y-Axis	0.17	188.50	0.36	154.50	0.53	127.50
HIC Z-Axis	0.77	77.50	1.28	119.00	2.64	106.50
Resultant HIC	11.57	124.00	16.91	104.50	24.36	90.00

***-Minus X / Plus Y ***

	7 G-Level	9 G-Level		
Run	LX4247	LX4263		
	HIC Nbr	Width	HIC Nbr	Width
HIC X-Axis	23.27	115.00	33.30	81.50
HIC Y-Axis	0.14	59.50	0.61	57.00
HIC Z-Axis	1.94	58.00	6.11	63.00
Resultant HIC	27.86	112.00	47.72	109.50



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